

A general theory of thermo-compositional adiabatic and diabatic convection

DRF/MDS: P. Tremblin, T. Padioleau, P. Kestener, E. Audit

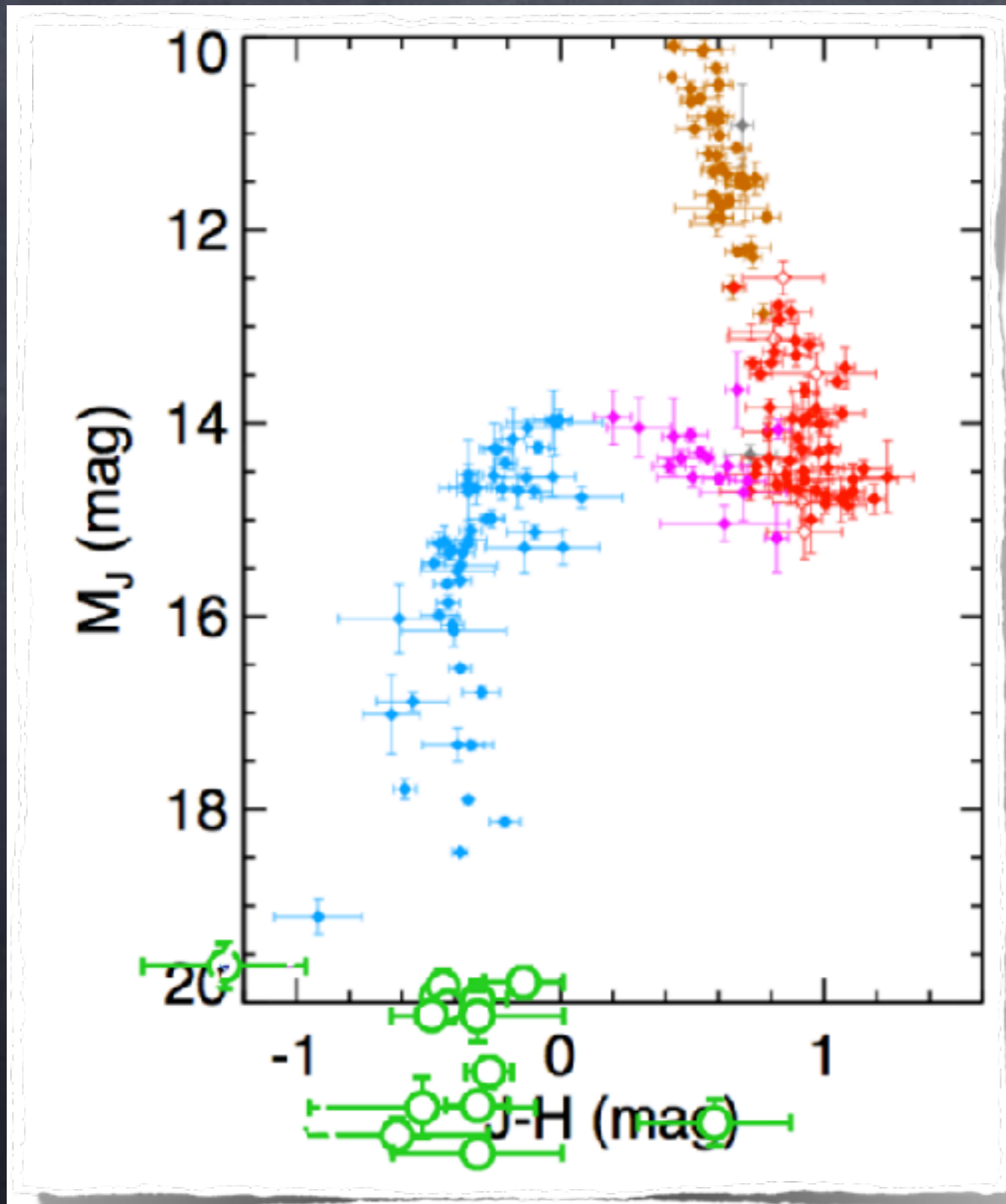
DEN/DANS/STMF: S. Kokh

DRF/IRFU/DAP: S. Fromang, P.-O. Lagage

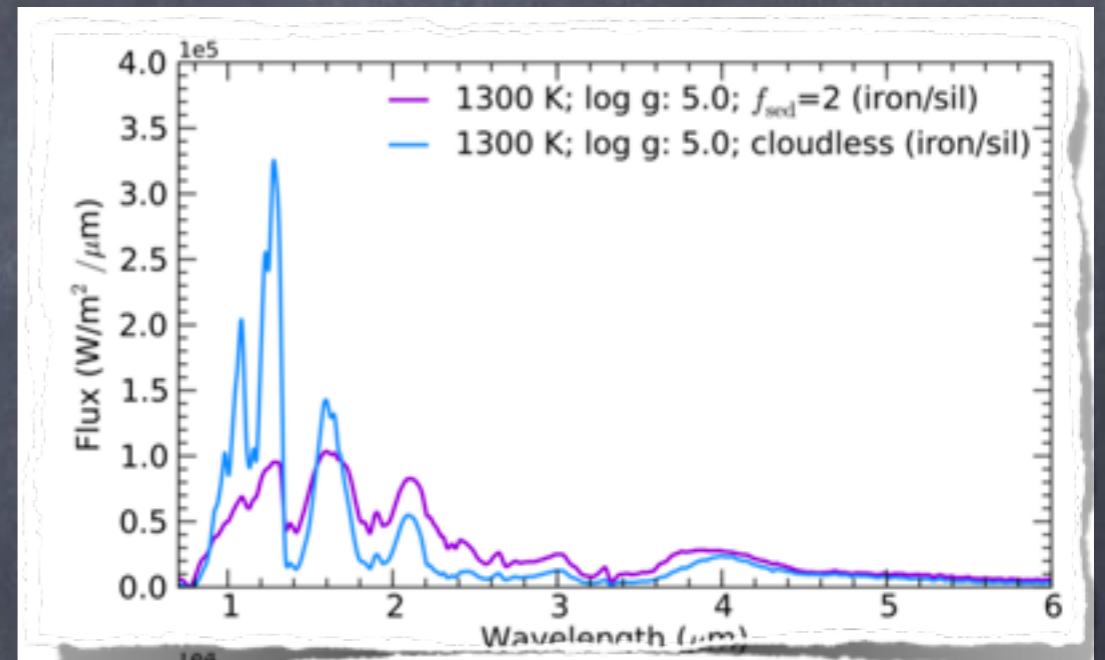
Exeter/Lyon: I. Baraffe, G. Chabrier, M. Phillips



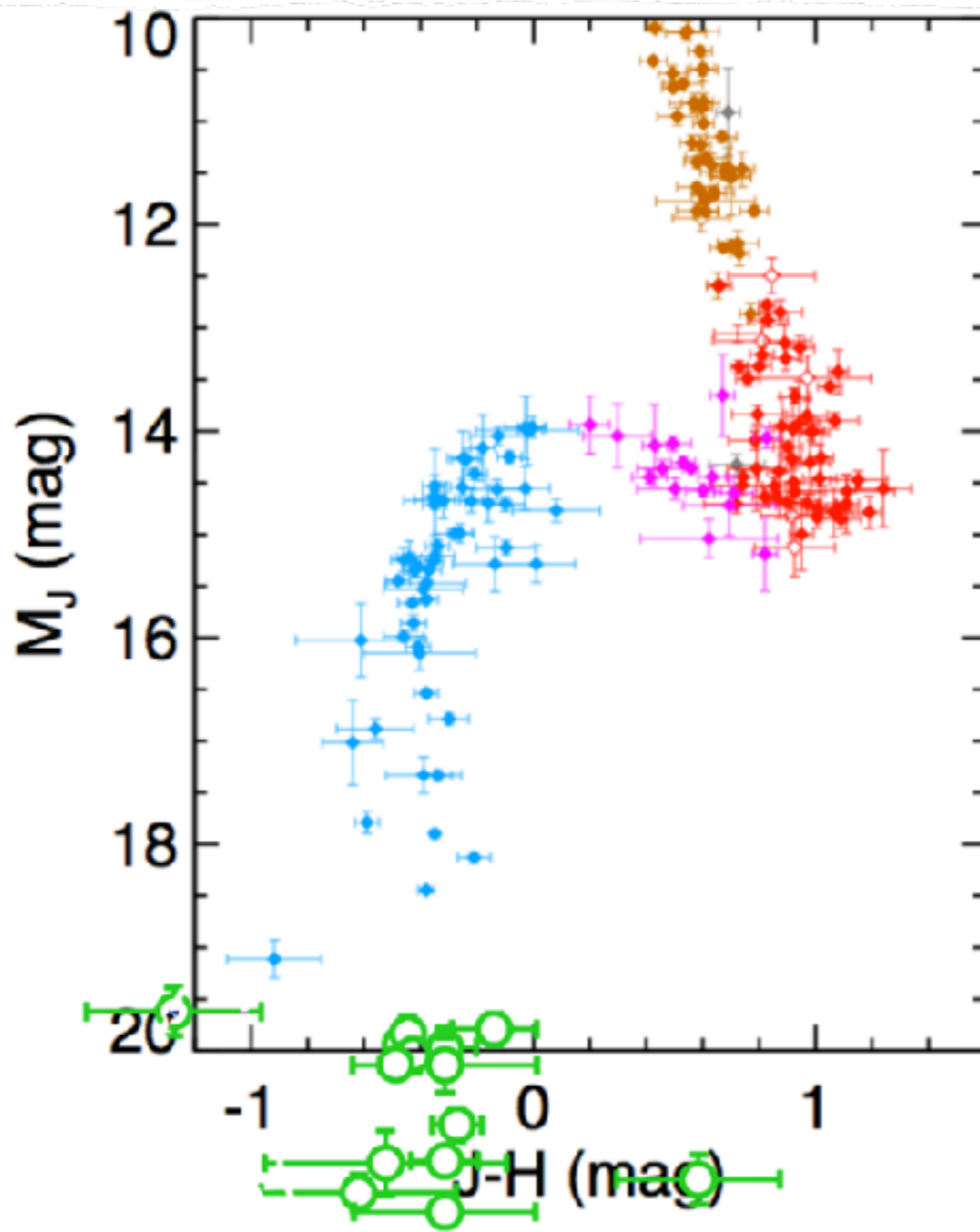
- Brown dwarfs spectral sequence:



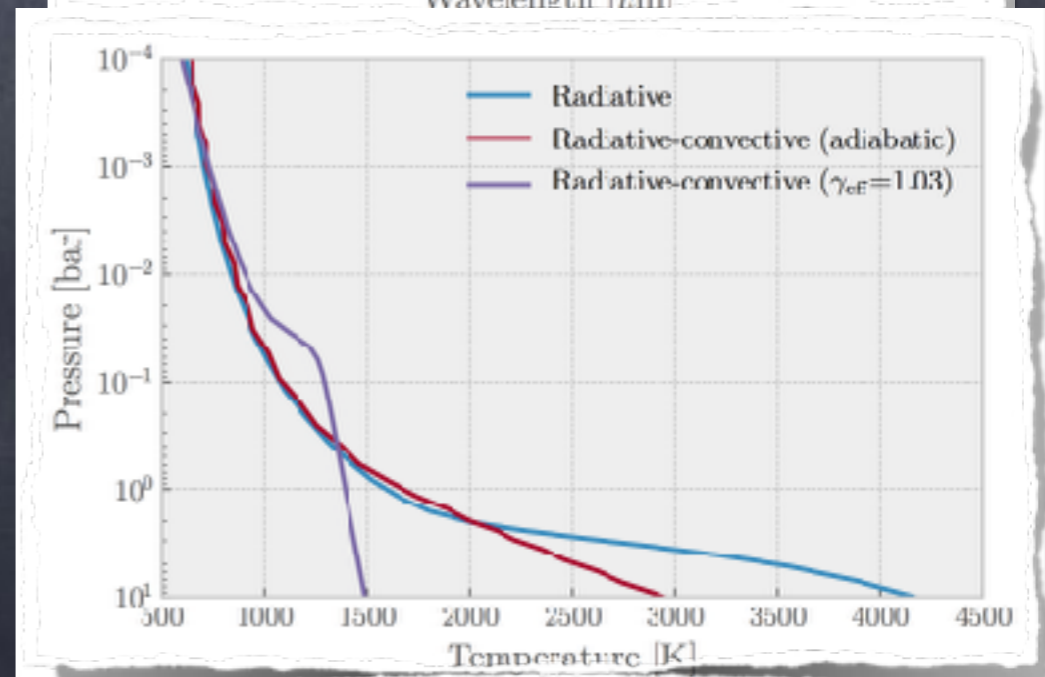
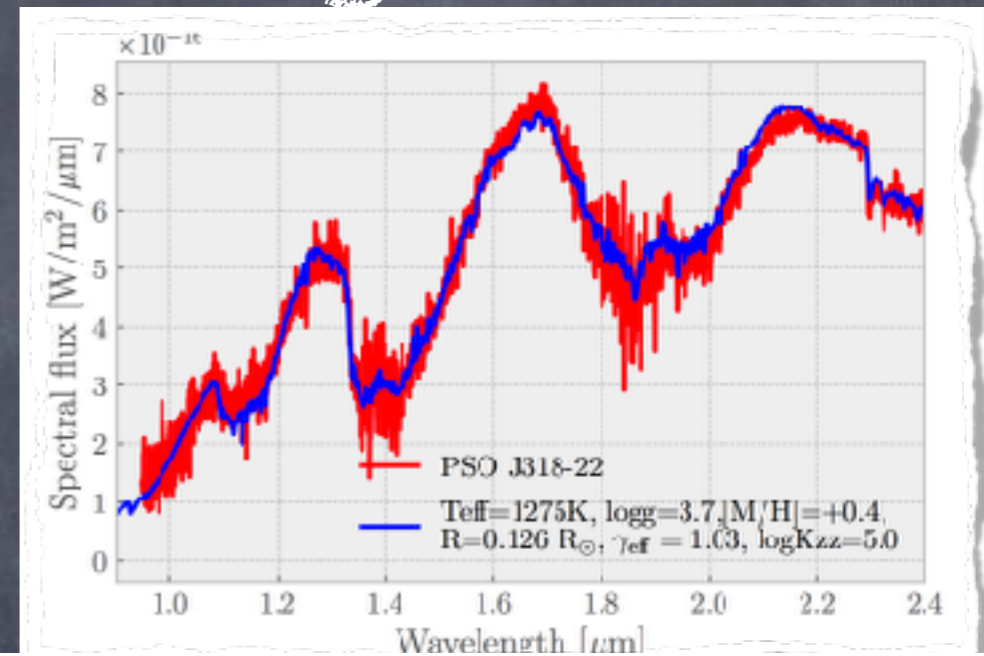
Clouds?



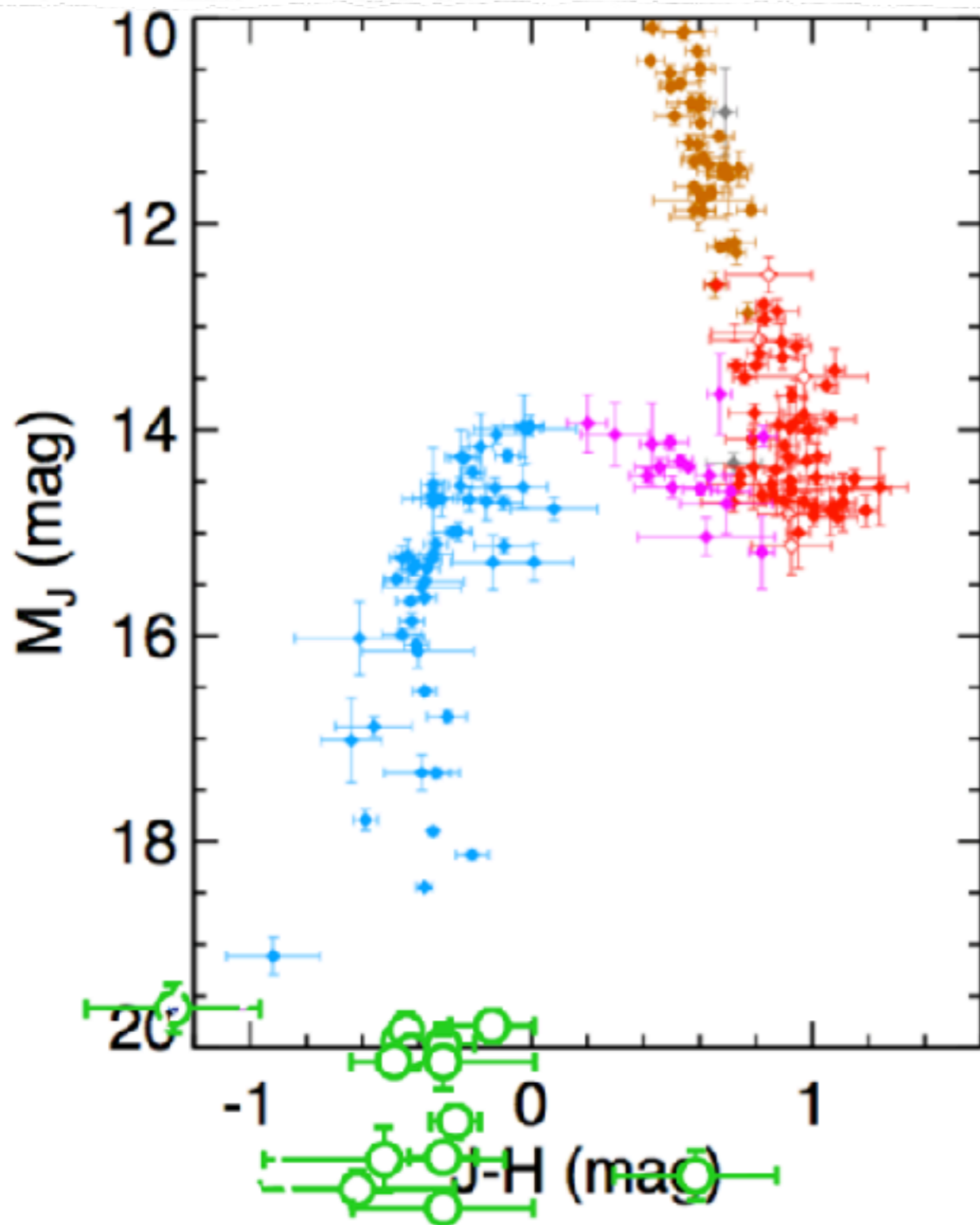
- Brown dwarfs spectral sequence:



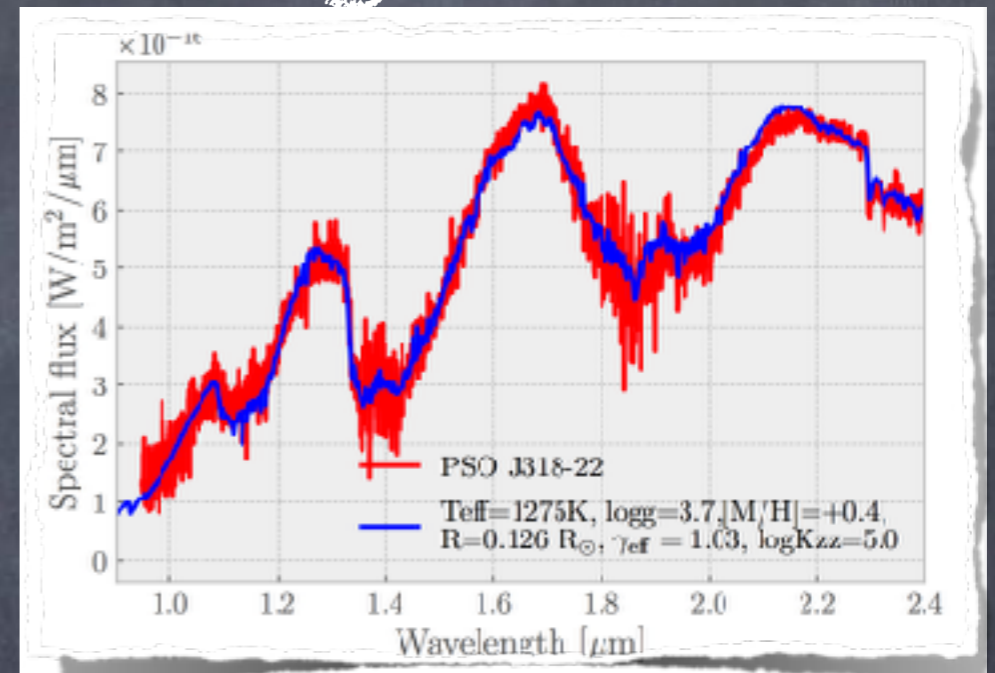
or reduced
T gradient?



- Brown dwarfs spectral sequence:



or reduced
T gradient?



Convection
linked to
CO/CH4 transition?

- Stratified compressible hydrodynamics

Numerical scheme, simulations and HPC
implementation

→ Thomas Padioleau

with P. Kestener CEA/MdLs: HPC

with S. Kokh CEA/DEN: numerical scheme

and E. Audit CEA/MdLs

- Stratified compressible hydrodynamics

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = 0$$

$$\frac{\partial \rho \vec{u}}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u} \otimes \vec{u} + P) = \rho \vec{g}$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + \vec{\nabla} \cdot (\vec{u} (\rho \mathcal{E} + P)) = \rho c_p H(X, T)$$

$$\frac{\partial \rho X}{\partial t} + \vec{\nabla} \cdot (\rho X \vec{u}) = \rho R(X, T)$$

$$\mathcal{E} = e + \frac{1}{2} u^2 + \phi$$

$$\vec{g} = -\vec{\nabla} \phi$$

$$P = e(\gamma - 1) = \rho k_b T / \mu(X)$$

- Stratified compressible hydrodynamics

- Compressibility/conservation

- finite volume scheme
- co-localised variables

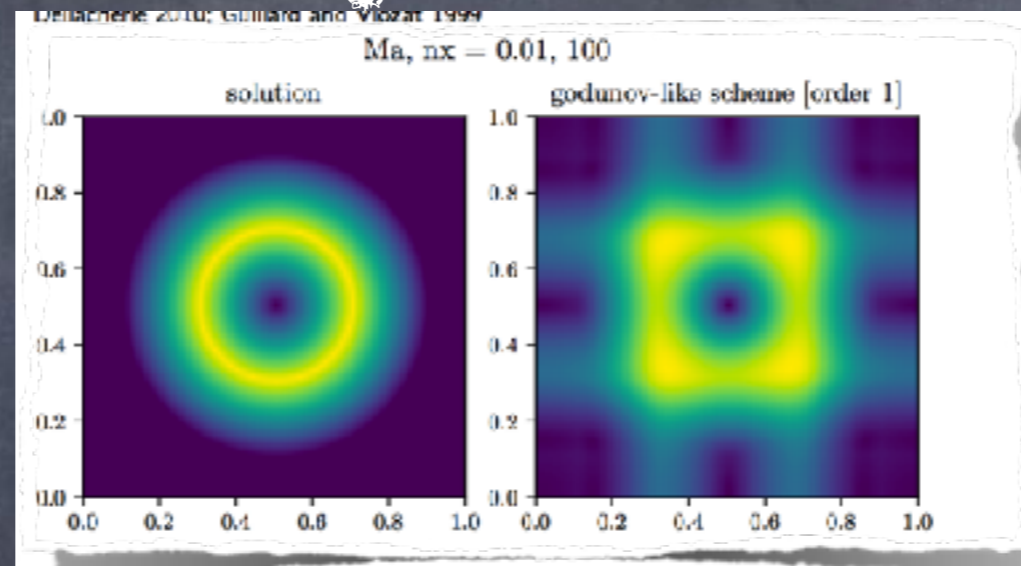
- Problems

- poor accuracy at low Mach
- small timestep ($dt = dx/c$)
- poor hydrostatic balance

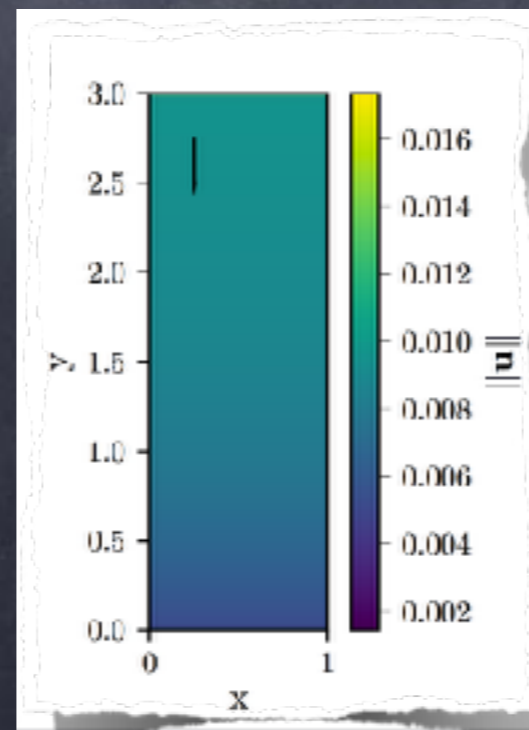
- Stratified compressible hydrodynamics

- Problems

- poor accuracy at low Mach



- poor hydrostatic balance



- Stratified compressible hydrodynamics
- ALL-regime solver: full scheme

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_x)}{\partial x} = 0$$

$$\frac{\partial \rho u_x}{\partial t} + \frac{\partial(\rho u_x^2 + P)}{\partial x} = 0$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + \frac{\partial((\rho \mathcal{E} + P)u_x)}{\partial x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: full scheme

$$\frac{\partial \rho}{\partial t} + \rho \frac{\partial u_x}{\partial x} + u_x \frac{\partial \rho}{\partial x} = 0$$

$$\frac{\partial \rho u_x}{\partial t} + \rho u_x \frac{\partial u_x}{\partial x} + \frac{\partial P}{\partial x} + u_x \frac{\partial \rho u_x}{\partial x} = 0$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + \rho \mathcal{E} \frac{\partial u_x}{\partial x} + \frac{\partial P u_x}{\partial x} + u_x \frac{\partial \rho \mathcal{E}}{\partial x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: acoustic step

$$\frac{\partial \rho}{\partial t} + \rho \frac{\partial u_x}{\partial x} = 0$$

$$\frac{\partial \rho u_x}{\partial t} + \rho u_x \frac{\partial u_x}{\partial x} + \frac{\partial P}{\partial x} = 0$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + \rho \mathcal{E} \frac{\partial u_x}{\partial x} + \frac{\partial P u_x}{\partial x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: acoustic step

$$\frac{\partial \tau}{\partial t} - \frac{\partial u_x}{\partial m} = 0$$

$$\frac{\partial u_x}{\partial t} + \frac{\partial P}{\partial m} = 0$$

$$\frac{\partial \mathcal{E}}{\partial t} + \frac{\partial P u_x}{\partial m} = 0$$

$$\tau = \frac{1}{\rho}$$

$$dm = \rho dx$$

- Stratified compressible hydrodynamics
- ALL-regime solver: acoustic step

$$\frac{\partial \tau}{\partial t} - \frac{\partial u_x}{\partial m} = 0$$

$$\frac{\partial u_x}{\partial t} + \frac{\partial \Pi}{\partial m} = 0$$

$$\frac{\partial \mathcal{E}}{\partial t} + \frac{\partial \Pi u_x}{\partial m} = 0$$

$$\frac{\partial \Pi}{\partial t} + a^2 \frac{\partial u_x}{\partial m} = 0$$

$$\tau = \frac{1}{\rho}$$

$$dm = \rho dx$$

$$a = \rho c_s$$

$$\Pi^{n+1-} = p(\tau^{n+1-}, \mathcal{E}^{n+1-}, u_x^{n+1-})$$

- Stratified compressible hydrodynamics
- ALL-regime solver: acoustic step

$$U_{i+1/2}^* = \frac{u_{x,i} + u_{x,i+1}}{2} - \frac{1}{2a} (\Pi_{i+1} - \Pi_i)$$

$$\Pi_{i+1/2}^* = \frac{\Pi_i + \Pi_{i+1}}{2} - \frac{a}{2} (u_{x,i+1} - u_{x,i})$$

- Stratified compressible hydrodynamics
- ALL-regime solver: acoustic step

$$U_{i+1/2}^* = \frac{u_{x,i} + u_{x,i+1}}{2} - \frac{1}{2a} (\Pi_{i+1} - \Pi_i)$$

$$\Pi_{i+1/2}^* = \frac{\Pi_i + \Pi_{i+1}}{2} - \frac{a}{2} (u_{x,i+1} - u_{x,i})$$

$$\frac{\tau^{n+1-} - \tau^n}{\Delta t} - \frac{U_{i+1/2}^* - U_{i-1/2}^*}{\Delta m} = 0$$

$$\frac{u_x^{n+1-} - u_x^n}{\Delta t} + \frac{\Pi_{i+1/2}^* - \Pi_{i-1/2}^*}{\Delta m} = 0$$

$$\frac{\mathcal{E}^{n+1-} - \mathcal{E}^n}{\Delta t} + \frac{U_{i+1/2}^* \Pi_{i+1/2}^* - U_{i-1/2}^* \Pi_{i-1/2}^*}{\Delta m} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: transport step

$$\frac{\partial \rho}{\partial t} + u_x \frac{\partial \rho}{\partial x} = 0$$

$$\frac{\partial \rho u_x}{\partial t} + u_x \frac{\partial \rho u_x}{\partial x} = 0$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + u_x \frac{\partial \rho \mathcal{E}}{\partial x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: transport step

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_x}{\partial x} - \rho \frac{\partial u_x}{\partial x} = 0$$

$$\frac{\partial \rho u_x}{\partial t} + \frac{\partial \rho u_x^2}{\partial x} - \rho u_x \frac{\partial u_x}{\partial x} = 0$$

$$\frac{\partial \rho \mathcal{E}}{\partial t} + \frac{\partial \rho \mathcal{E} u_x}{\partial x} - \rho \mathcal{E} \frac{\partial u_x}{\partial x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: transport step

$$\frac{\rho^{n+1} - \rho^{n+1-}}{\Delta t} + \frac{[\rho^{n+1-} U^*]}{\Delta x} - \rho^{n+1-} \frac{[U^*]}{\Delta x} = 0$$

$$\frac{(\rho u_x)^{n+1} - (\rho u_x)^{n+1-}}{\Delta t} + \frac{[(\rho u_x)^{n+1-} U^*]}{\Delta x} - (\rho u_x)^{n+1-} \frac{[U^*]}{\Delta x} = 0$$

$$\frac{(\rho \mathcal{E})^{n+1} - (\rho \mathcal{E})^{n+1-}}{\Delta t} + \frac{[(\rho \mathcal{E})^{n+1-} U^*]}{\Delta x} - (\rho \mathcal{E})^{n+1-} \frac{[U^*]}{\Delta x} = 0$$

- Stratified compressible hydrodynamics
- ALL-regime solver: full scheme

$$\frac{\rho^{n+1} - \rho^n}{\Delta t} + \frac{[\rho^{n+1} - U^*]}{\Delta x} = 0$$

$$\frac{(\rho u_x)^{n+1} - (\rho u_x)^n}{\Delta t} + \frac{[(\rho u_x)^{n+1} - U^* + \Pi^*]}{\Delta x} = 0$$

$$\frac{(\rho \mathcal{E})^{n+1} - (\rho \mathcal{E})^n}{\Delta t} + \frac{[(\rho \mathcal{E})^{n+1} - U^* + \Pi^* U^*]}{\Delta x} = 0$$

$$U_{i+1/2}^* = \frac{u_{x,i} + u_{x,i+1}}{2} - \frac{1}{2a} (\Pi_{i+1} - \Pi_i)$$

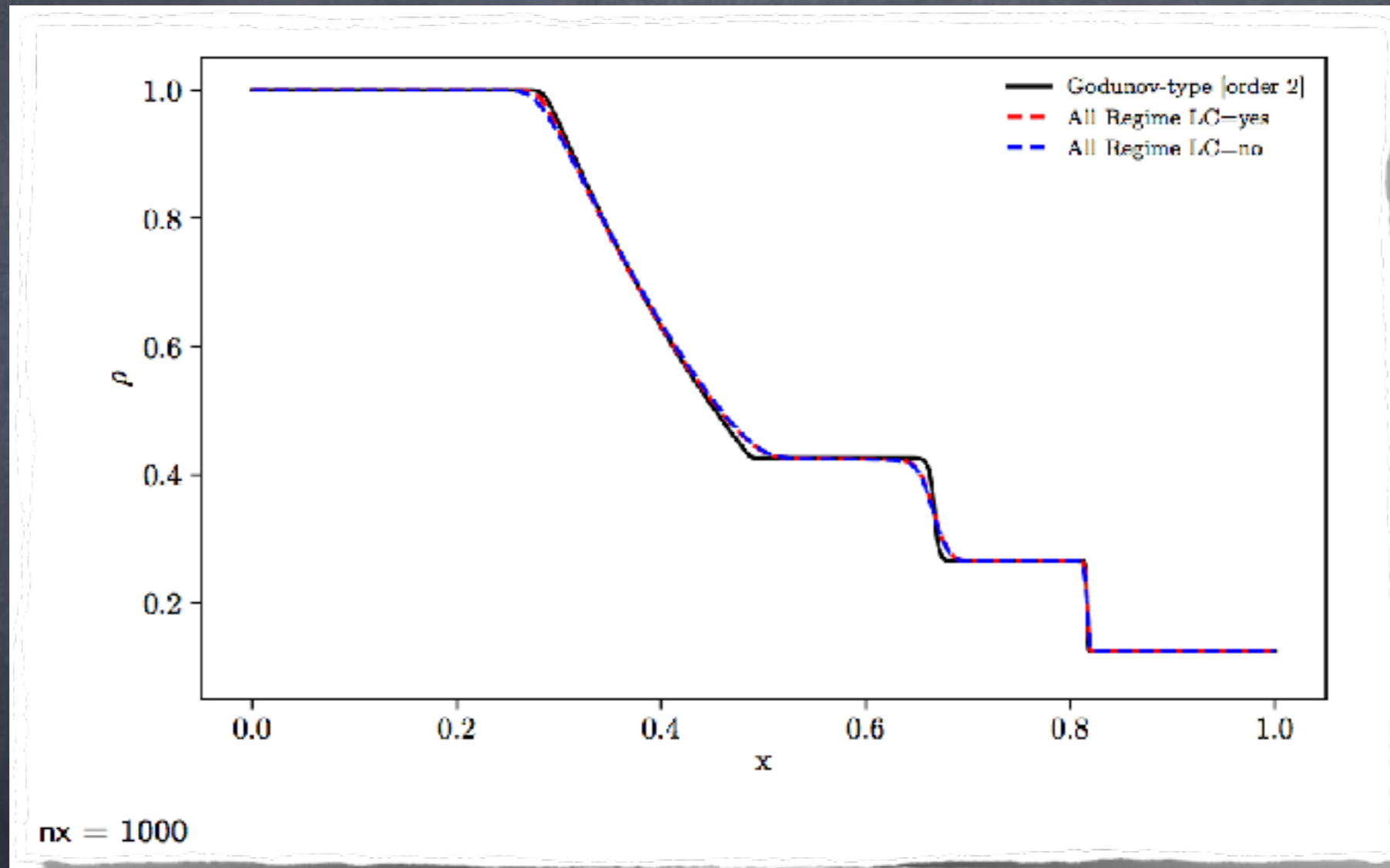
$$\Pi_{i+1/2}^* = \frac{\Pi_i + \Pi_{i+1}}{2} - \frac{a}{2} (u_{x,i+1} - u_{x,i})$$

- Stratified compressible hydrodynamics
 - All-regime solver: full scheme
 - Explicit/Explicit scheme
 - Implicit/Explicit scheme
 - Low Mach correction

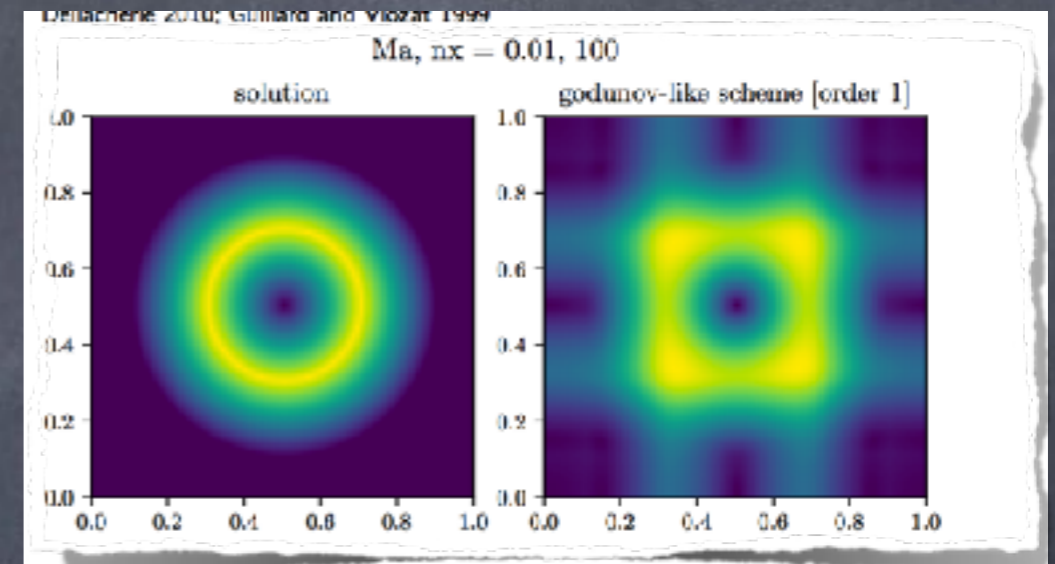
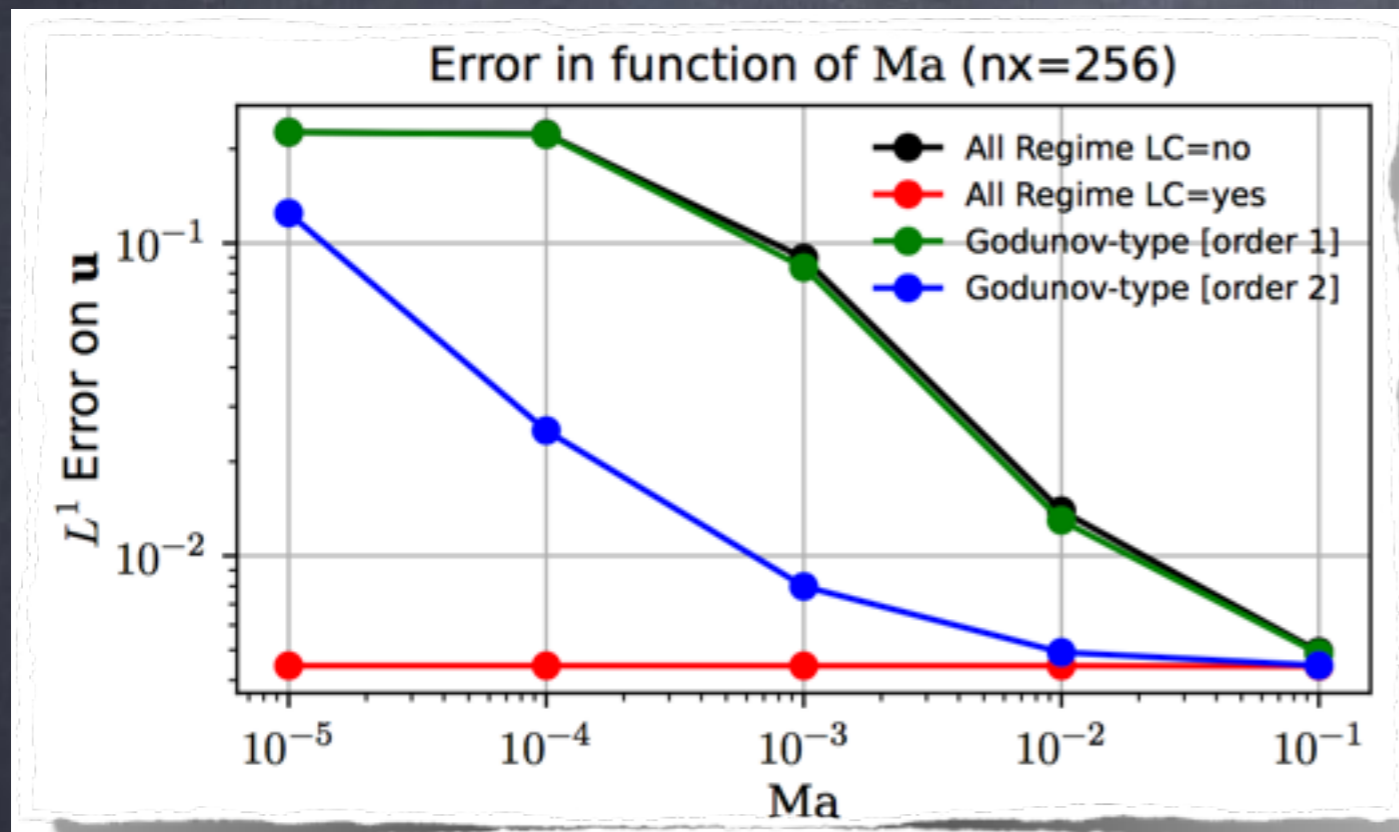
$$U_{i+1/2}^{\star} = \frac{u_{x,i} + u_{x,i+1}}{2} - \frac{1}{2a} (\Pi_{i+1} - \Pi_i)$$

$$\Pi_{i+1/2}^{\star} = \frac{\Pi_i + \Pi_{i+1}}{2} - \frac{a}{2} (u_{x,i+1} - u_{x,i})$$

- Stratified compressible hydrodynamics
 - ALL-regime solver: full scheme
 - conservative scheme: Sod test



- Stratified compressible hydrodynamics
 - ALL-regime solver: full scheme
 - Low Mach correction: Gresho vortex



- Stratified compressible hydrodynamics
- ALL-regime solver with gravity
- hydrostatic balance at cell centre

$$\frac{(\rho u_x)^{n+1} - (\rho u_x)^n}{\Delta t} + \frac{[(\rho u_x)^{n+1} - U^* + \Pi^*]}{\Delta x} = -\rho g$$

if there is initially no velocity

$$\frac{\Pi_i + \Pi_{i+1}}{2} - \frac{\Pi_i + \Pi_{i-1}}{2} = -\rho_i g \Delta x$$

$$u_x^{n+1} = O(\Delta x), \quad \frac{\partial P}{\partial x} = -\rho g + O(\Delta x)$$

- Stratified compressible hydrodynamics
- **All-regime solver with gravity**
- hydrostatic balance at interface

$$\frac{(\rho u_x)^{n+1} - (\rho u_x)^n}{\Delta t} + \frac{[(\rho u_x)^{n+1} - U^* + \Pi^*]}{\Delta x} = -\frac{1}{2} \left(\frac{\rho_i + \rho_{i+1}}{2} + \frac{\rho_i + \rho_{i-1}}{2} \right) g$$

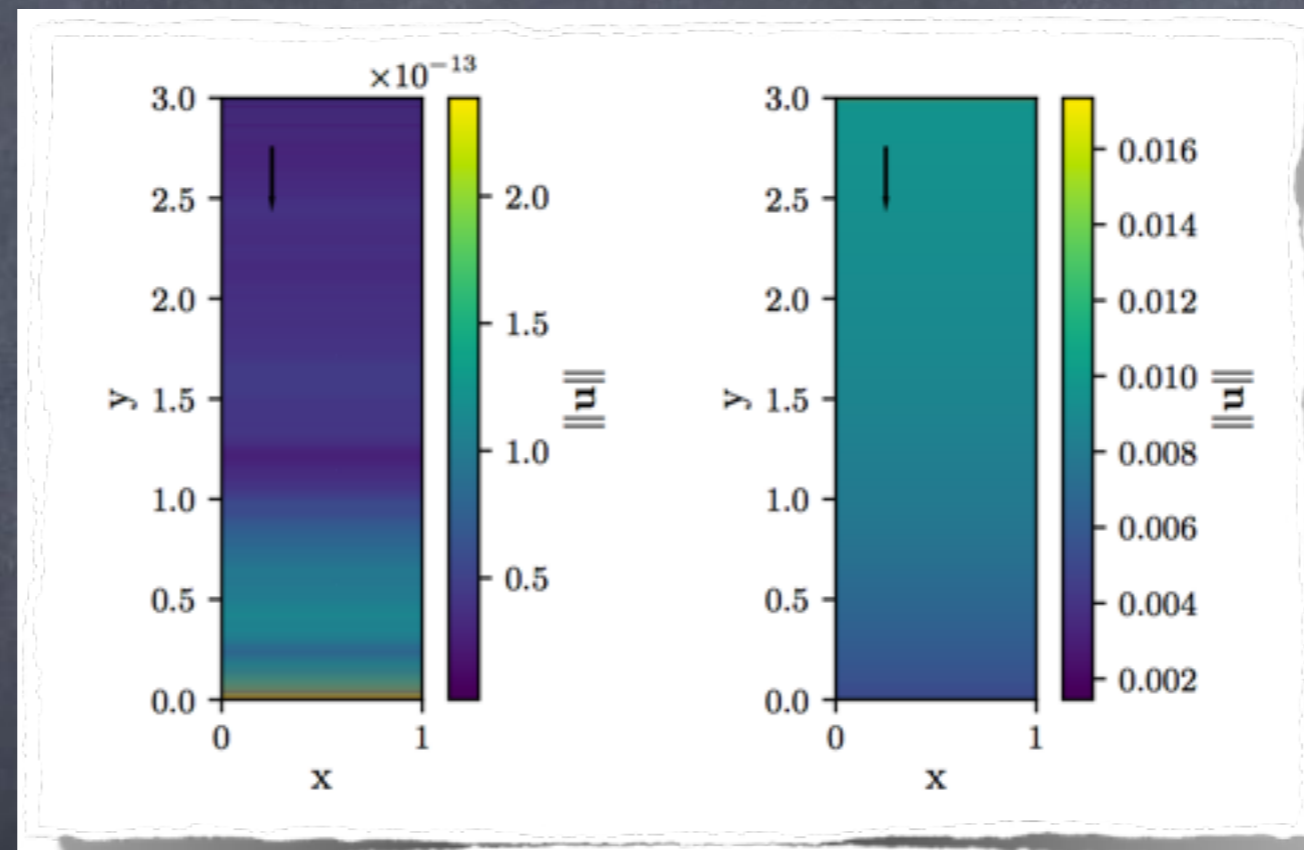
if there is initially no velocity

$$\frac{\Pi_i + \Pi_{i+1}}{2} - \frac{\Pi_i + \Pi_{i-1}}{2} = -\frac{1}{2} \left(\frac{\rho_i + \rho_{i+1}}{2} + \frac{\rho_i + \rho_{i-1}}{2} \right) g \Delta x$$

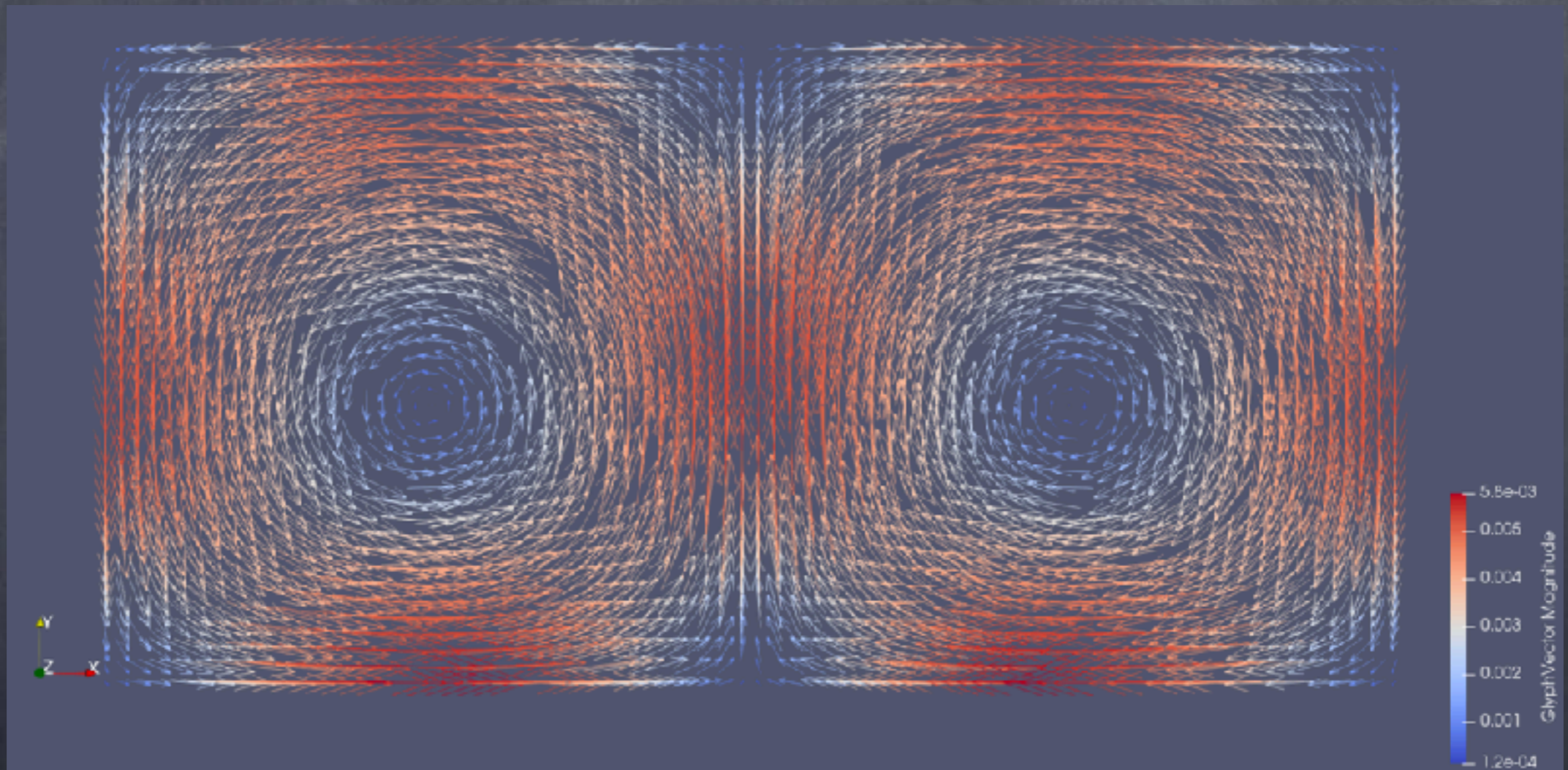
$$\Pi_{i+1} - \Pi_i = \frac{\rho_i + \rho_{i+1}}{2} g \Delta x \quad \Pi_i - \Pi_{i-1} = \frac{\rho_{i-1} + \rho_i}{2} g \Delta x$$

$$u_x^{n+1} = 0, \quad \frac{\partial P}{\partial x} = -\rho g$$

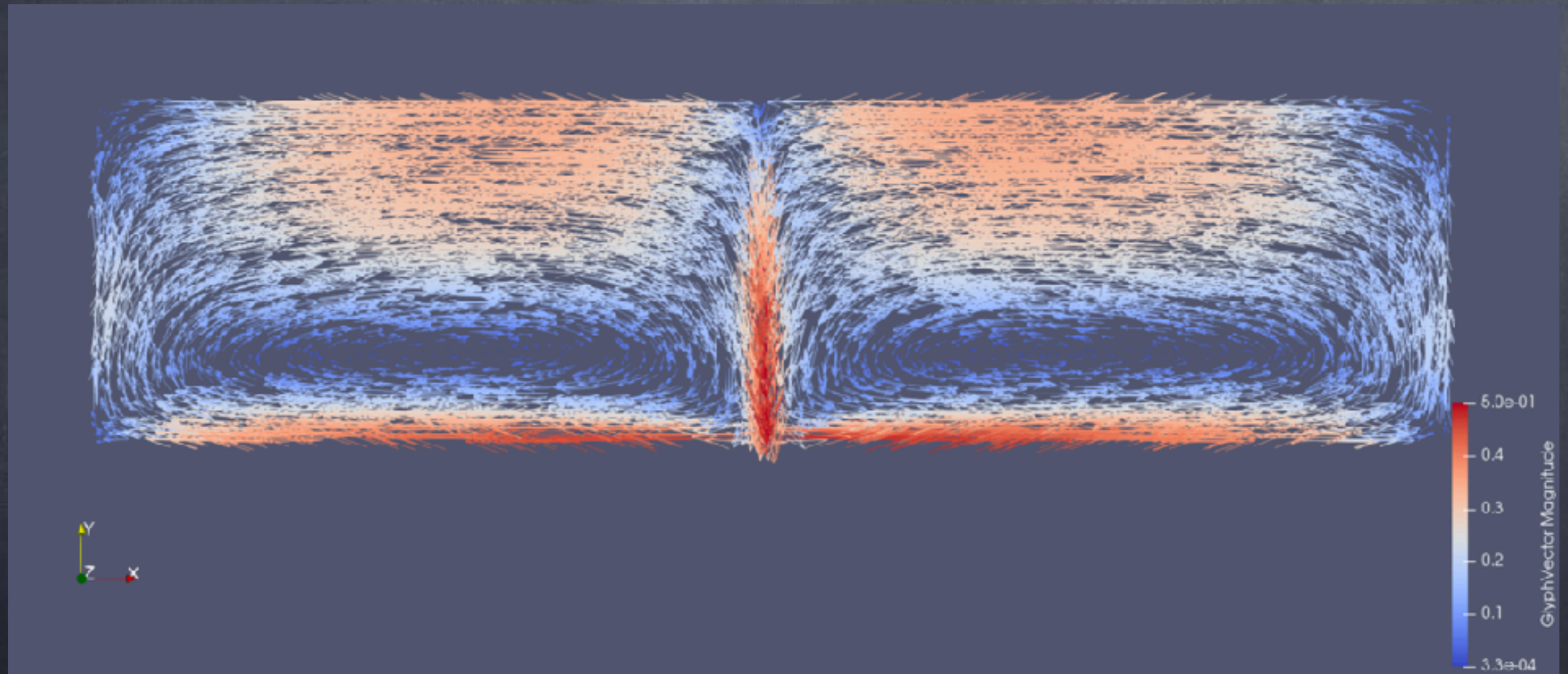
- Stratified compressible hydrodynamics
 - ALL-regime solver with gravity
 - hydrostatic balance at interface



- Stratified compressible hydrodynamics
 - All-regime solver with gravity
 - Convective simulation
 - Low Mach correction



- Stratified compressible hydrodynamics
 - All-regime solver with gravity
 - Compressible convective simulation



- Stratified compressible hydrodynamics
 - ALL-regime solver with gravity
 - Parallel HPC Implementation



Problem of portability and performance probability....

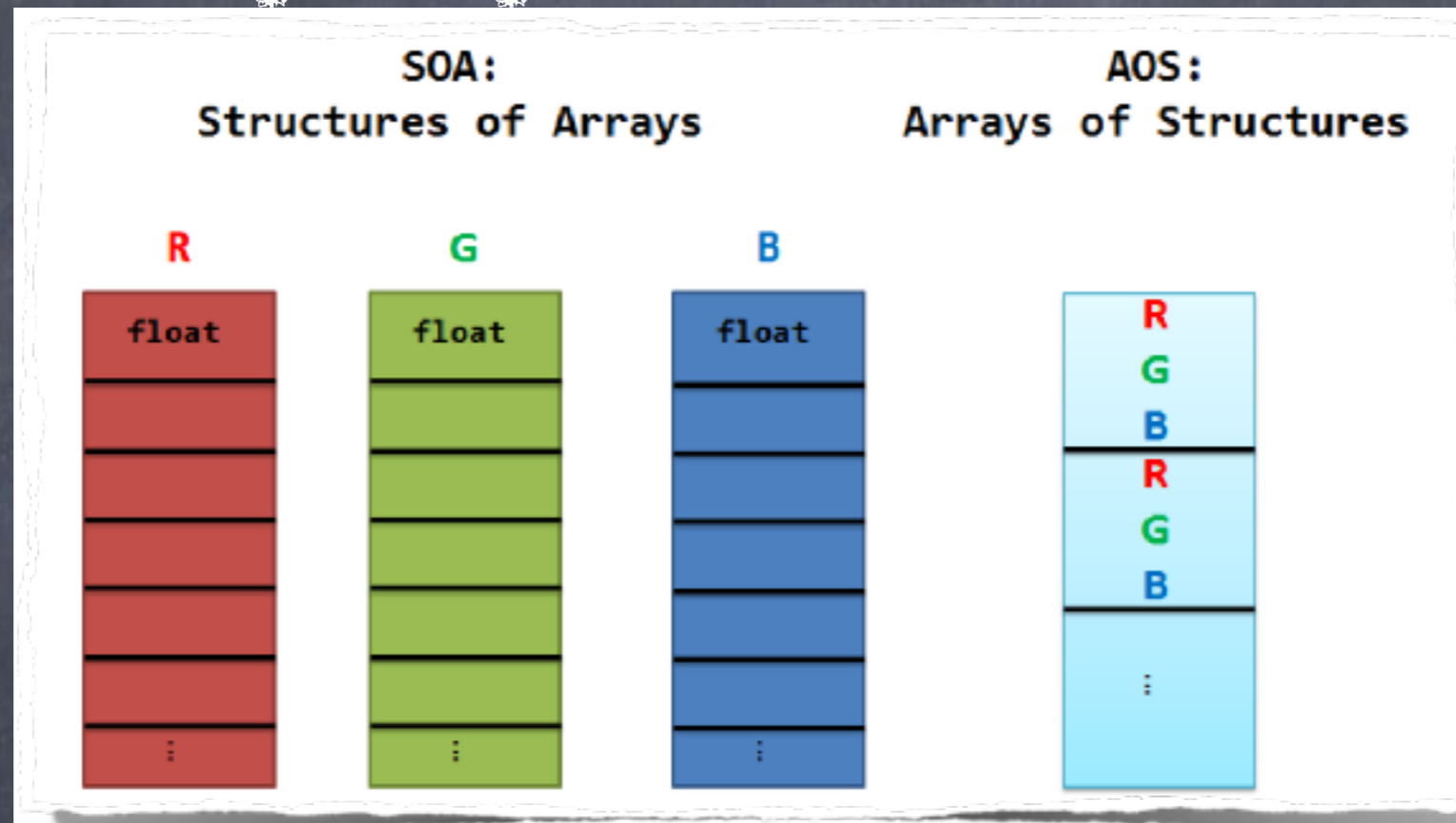
- Stratified compressible hydrodynamics
 - ALL-regime solver with gravity
 - Parallel HPC Implementation



Kokkos Library:

- C++ Library for perf. portability
- extracted from Trilinos (Sandia)
- backend: openMP, Pthreads, CUDA
- abstraction of memory space and execution space

- Stratified compressible hydrodynamics
- ALL-regime solver with gravity
- Memory layout:



```
// Old matrix type:  
// typedef View<double**,Device> my_matrix ;  
  
// Change matrix type to an 8x8 tiled layout.  
typedef View< double** ,  
            LayoutTileLeft<8,8> ,  
            Device > my_matrix ;
```

- Stratified compressible hydrodynamics
 - ALL-regime solver with gravity
 - Kokkos kernel

```
struct InitView
{
  InitView(Kokkos::View<double*[3]> a)
    : m_a(a)
  {}

  KOKKOS_INLINE_FUNCTION
  void operator()(const int i) const
  {
    a(i, 0) = 1.0*i;
    a(i, 1) = 1.0*i*i;
    a(i, 2) = 1.0*i*i*i;
  }

  Kokkos::View<double*[3]> m_a;
};
```

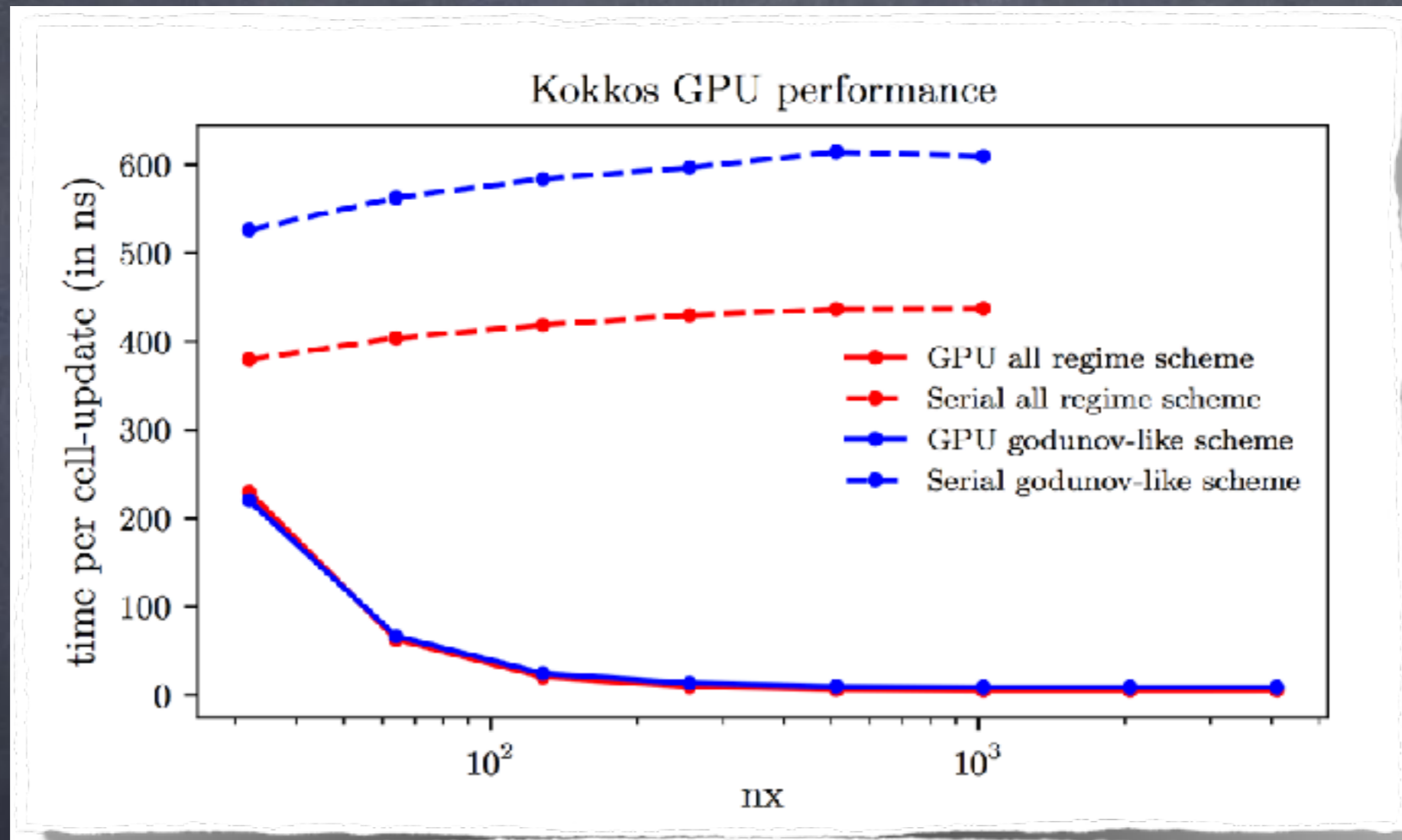
```
int main (int argc, char* argv[])
{
  Kokkos::initialize(argc, argv);

  Kokkos::View<double*[3]> view("View_name", 15);

  Kokkos::parallel_for(15, InitView(view));

  Kokkos::finalize();
}
```

- Stratified compressible hydrodynamics
- ALL-regime solver with gravity
- Kokkos kernel



- Stratified compressible hydrodynamics
- ALL-regime solver with gravity
- 2D diabatic convection

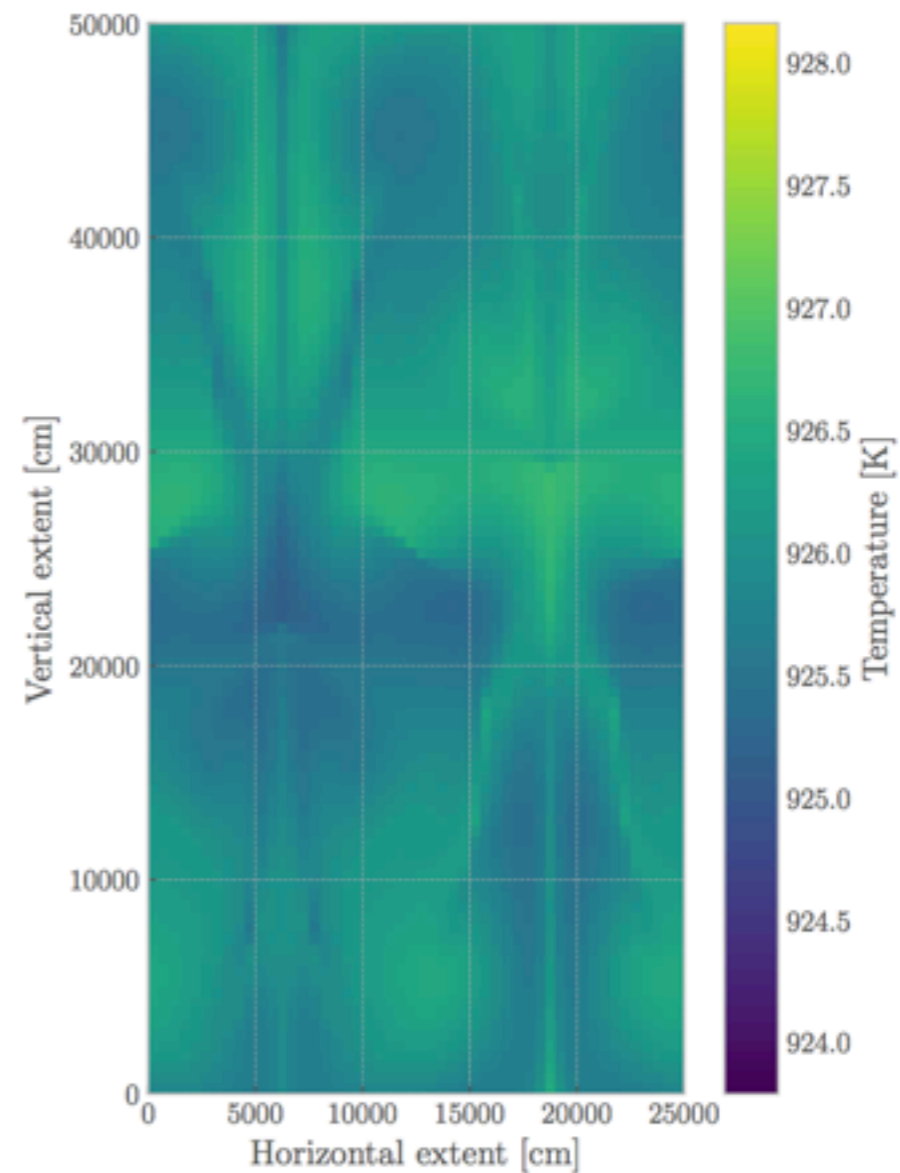
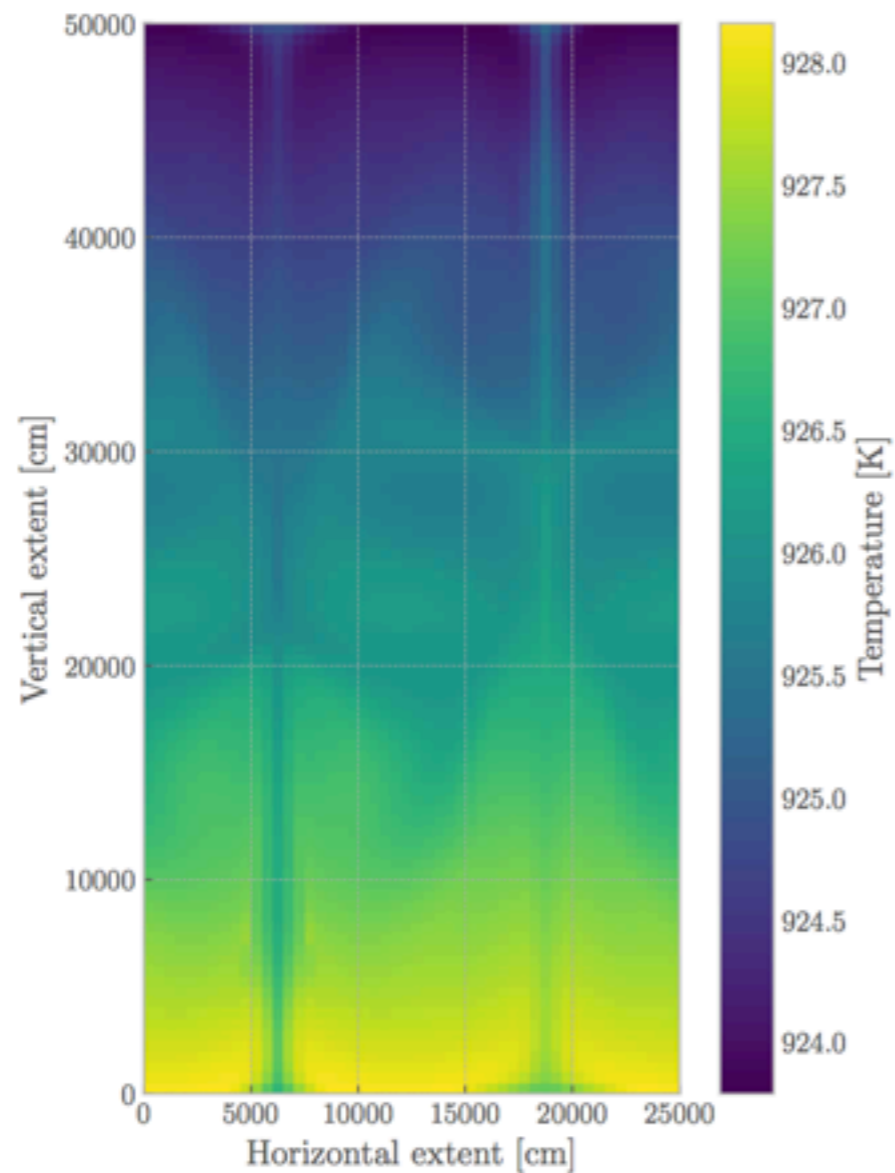
$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = 0$$

$$\frac{\partial \rho \vec{u}}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u} \otimes \vec{u} + P) = \rho \vec{g}$$

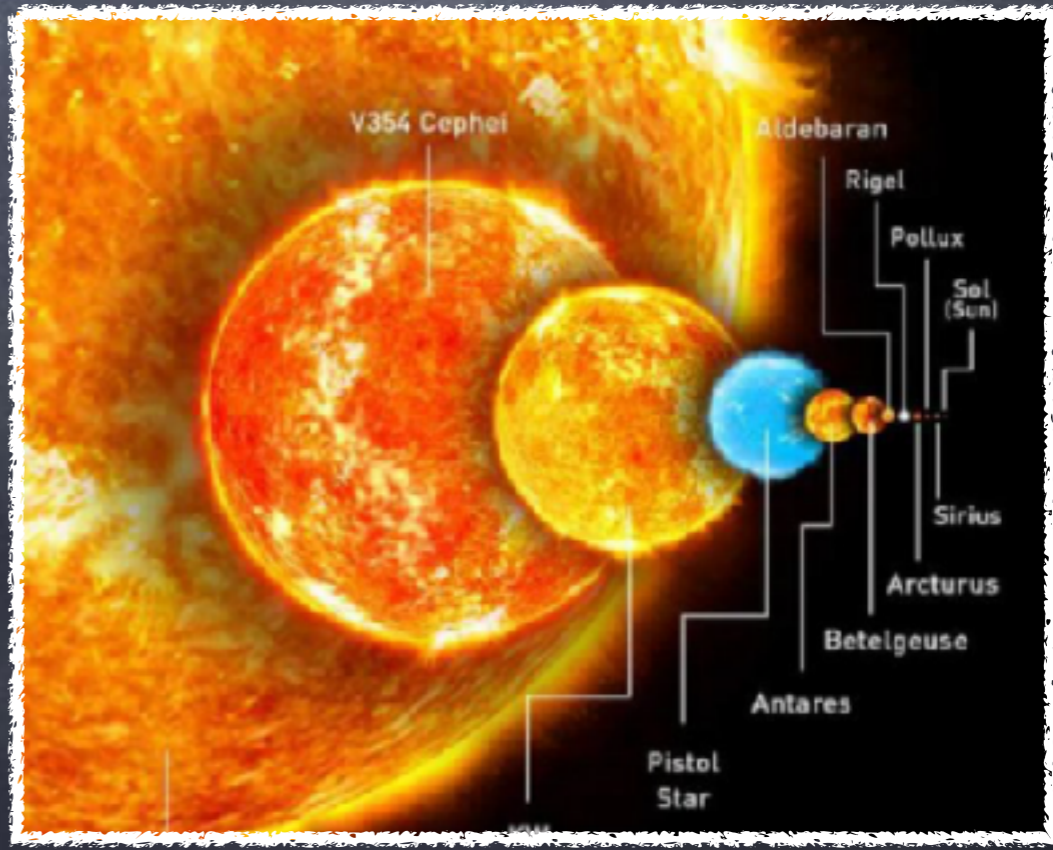
$$\frac{\partial \rho \mathcal{E}}{\partial t} + \vec{\nabla} \cdot (\vec{u} (\rho \mathcal{E} + P)) = \rho c_p H(X, T)$$

$$\frac{\partial \rho X}{\partial t} + \vec{\nabla} \cdot (\rho X \vec{u}) = \rho R(X, T)$$

- Stratified compressible hydrodynamics
- ALL-regime solver with gravity
- 2D diabatic convection



- What is in common between:

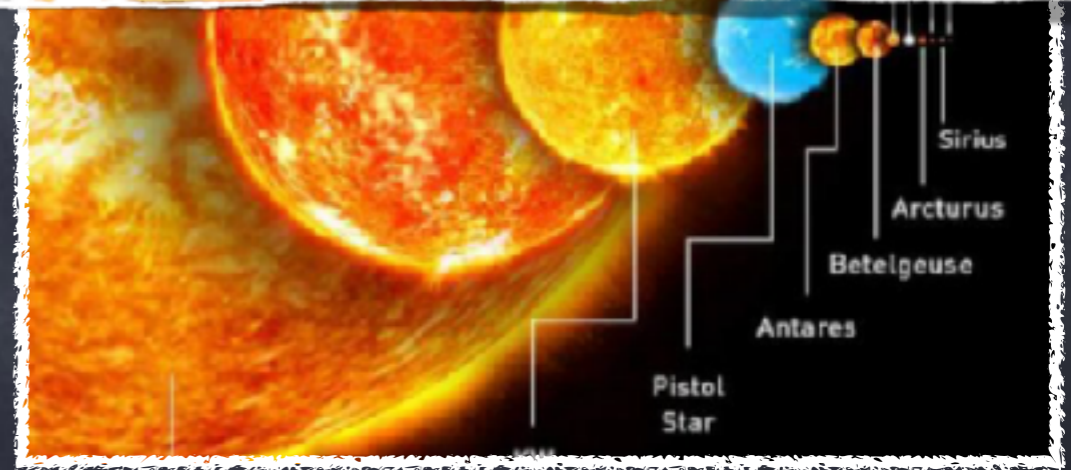


- What is in common between:



Convective systems but **not adiabatic**, they are all subject to:

- **Energy exchange** (latent heat, thermal diffusion, radiative transfer)
- and/or **compositional source terms** (chemical reactions, condensation/evaporation, compositional diffusion)



- What is adiabatic convection?

- Thermal adiabatic case

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = 0$$

$$\theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$P = \rho k_b T / \mu$$

- What is adiabatic convection?

- Thermal adiabatic case

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = 0$$

$$\theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$P = \rho k_b T / \mu$$

- Unstable if: $\frac{\partial \ln \theta_0}{\partial z} < 0$



- Schwarzschild criterion
(1906)

$$\nabla_T - \nabla_{\text{ad}} > 0, \quad \nabla_T = \frac{\partial \ln T_0}{\partial \ln P_0}$$

$$\frac{\partial T_0}{\partial z} < \frac{g}{C_p}$$

- What is adiabatic convection?

- Thermo-compositional adiabatic case

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = 0$$

$$\theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \vec{\nabla} (X) = 0$$

$$P = \rho k_b T / \mu(X)$$

- What is adiabatic convection?

- Thermo-compositional adiabatic case

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = 0 \quad \theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \vec{\nabla} (X) = 0 \quad P = \rho k_b T / \mu(X)$$

- Unstable if: $\nabla_T - \nabla_{\text{ad}} - \nabla_{\mu} > 0$



$$\nabla_T = \frac{\partial \ln T_0}{\partial \ln P_0}, \quad \nabla_{\mu} = \frac{\partial \ln \mu_0}{\partial \ln P_0}$$

- Ledoux criterion
(1947)

- What is ~~a~~ adiabatic convection?

- Thermo-compositional adiabatic case

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = \frac{H(X, T)}{T} \quad \theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \vec{\nabla} (X) = R(X, T) \quad P = \rho k_b T / \mu(X)$$

- What is **adiabatic convection**?

- **Thermo-compositional adiabatic case**

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = \frac{H(X, T)}{T} \quad \theta = T(P_{\text{ref}}/P)^{(\gamma-1)/\gamma}$$

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \vec{\nabla} (X) = R(X, T) \quad P = \rho k_b T / \mu(X)$$

- **Unstable if:** $\nabla_T - \nabla_{\text{ad}} - \nabla_{\mu} > 0$

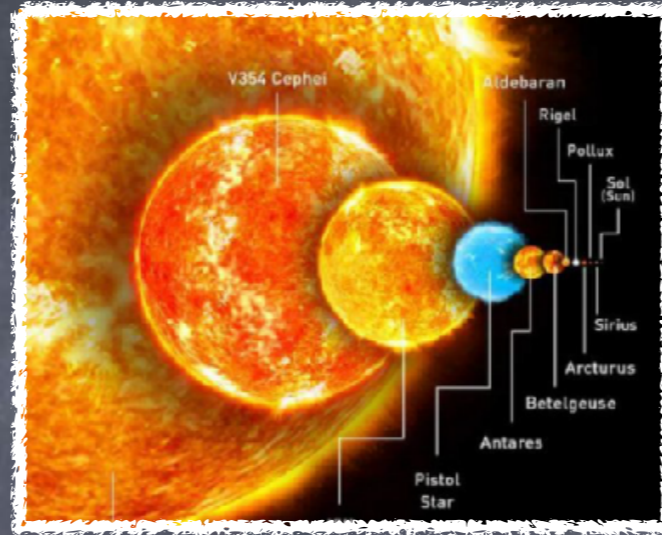
or

$$(\nabla_T - \nabla_{\text{ad}})\omega'_X - \nabla_{\mu}\omega'_T < 0$$

with $\omega'_X = R_X + R_T(T_0 \partial \ln \mu_0 / \partial X)$

and $\omega'_T = H_T + H_X(T_0 \partial \ln \mu_0 / \partial X)^{-1}$

- Thermohaline or fingering convection



$$(\nabla_T - \nabla_{\text{ad}})\omega'_X - \nabla_\mu \omega'_T < 0$$

with $R = \kappa_\mu \Delta X$ $\omega'_X = -k^2 \kappa_\mu$ ($R_T = 0$)

and $H = \kappa_T \Delta T$ $\omega'_T = -k^2 \kappa_T$ ($H_X = 0$)



Stern 1960

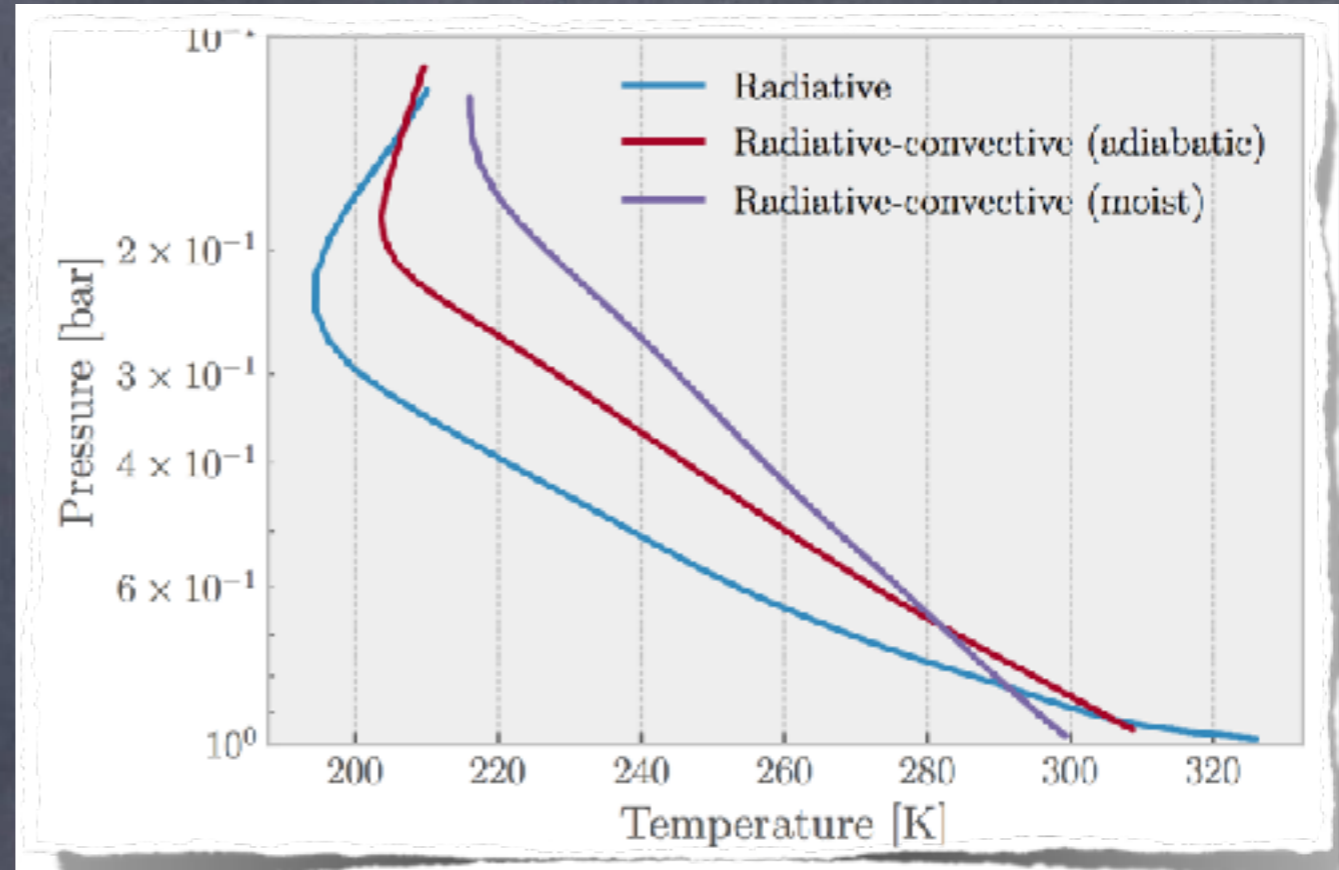


Ulrich 1972

$$(\nabla_T - \nabla_{\text{ad}})\kappa_\mu - \nabla_\mu \kappa_T > 0$$

and simulations from
 Traxler et al. 2011, Brown et al. 2013
 Garaud et al. 2015, Sengupta &
 Garaud 2018

- Steam/Liquid or moist convection



von Bezold 1893

$$\nabla_T - \nabla_{ad} > 0$$

Dry adiabat

$$\nabla_T - \nabla_{ad} \frac{1 + \frac{X_{eq}L}{R_d T_0}}{1 + \frac{X_{eq}L^2}{c_p R_v T_0^2}} > 0$$

Moist « pseudo-adiabat »

- Steam/Liquid or moist convection



$$(\nabla_T - \nabla_{\text{ad}})\omega'_X - \nabla_\mu \omega'_T < 0$$

with $R = R_{\text{cond}}(X, T)$ and $X = X_{\text{eq}}(P, T)$

and $H = -R_{\text{cond}}L/c_p$



von Bezold 1893

$$\nabla_T - \nabla_{\text{ad}} \frac{1 - \rho_0 \frac{\partial X_{\text{eq}}}{\partial P} L}{1 + \frac{\partial X_{\text{eq}}}{\partial T} \frac{L}{c_p}} > 0$$

Moist « pseudo-adiabat »

- Steam/Liquid or moist convection



$$(\nabla_T - \nabla_{\text{ad}})\omega'_X - \nabla_\mu \omega'_T < 0$$

with $R = R_{\text{cond}}(X, T)$ and $X = X_{\text{eq}}(P, T)$

and $H = -R_{\text{cond}}L/c_p$

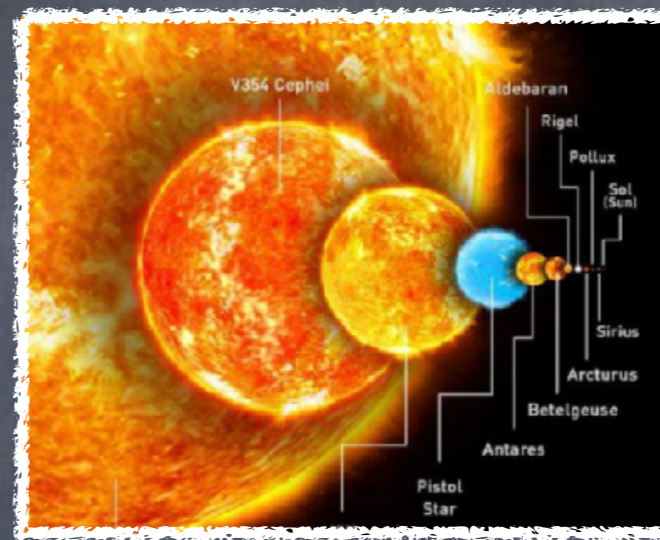


von Bezold 1893

$$\nabla_T - \nabla_{\text{ad}} \frac{1 - \rho_0 \frac{\partial X_{\text{eq}}}{\partial P} L}{1 + \frac{\partial X_{\text{eq}}}{\partial T} \frac{L}{c_p}} > 0$$

Moist « pseudo-adiabat »

- Thermo-compositional diabatic convection



Moist

Steam/Liquid

Fingering

Thermohaline



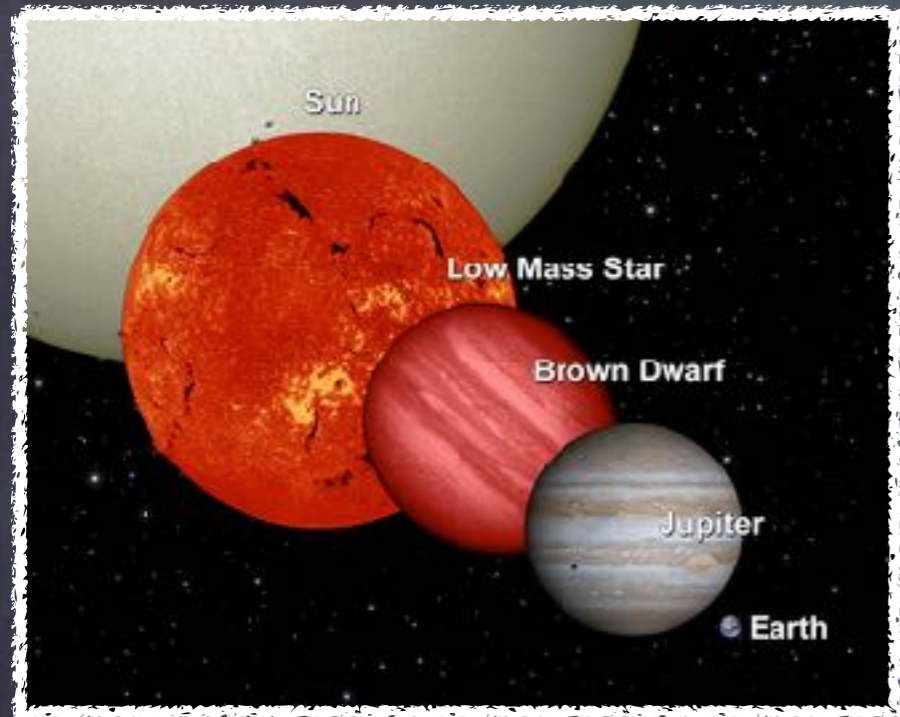
$$(\nabla_T - \nabla_{ad})\omega'_X - \nabla_\mu \omega'_T < 0$$

with $\omega'_X = R_X + R_T(T_0 \partial \ln \mu_0 / \partial X)$

and $\omega'_T = H_T + H_X(T_0 \partial \ln \mu_0 / \partial X)^{-1}$

and probably many more....

- CO/CH4 radiative convection

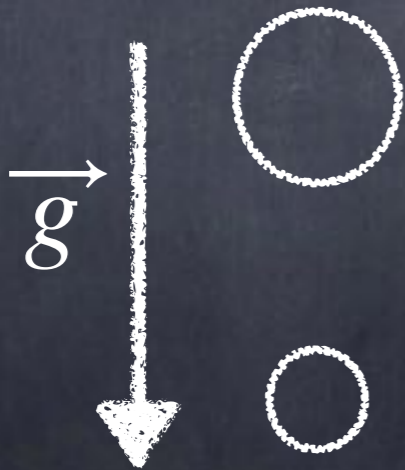


$$(\nabla_T - \nabla_{\text{ad}})\omega'_X - \nabla_\mu \omega'_T < 0$$

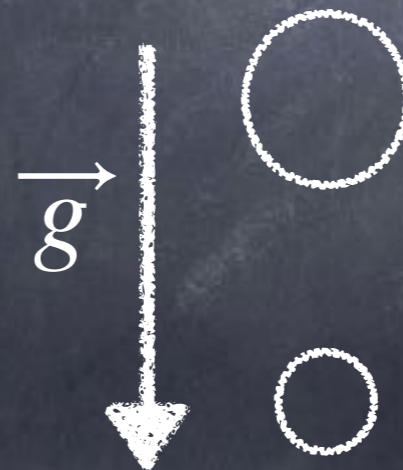
with $R = -(X - X_{\text{eq}})/\tau_{\text{chem}}$

and $H = 4\pi\kappa/c_p (J - \sigma T^4)$

Brown dwarfs and giant exoplanets



Moist convection



CO/CH4 radiative convection

- Generalisation of mixing length theory

$$\frac{\partial \ln \theta}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta) = \omega'_T \frac{\delta T}{T_0}$$

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \vec{\nabla} (X) = \omega'_X \delta X$$

$$\delta X \partial \ln \mu_0 / \partial X = \delta T / T_0$$

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$$\frac{\partial \ln \theta'}{\partial t} + \vec{u} \cdot \vec{\nabla} (\ln \theta') = 0$$

$$\text{with } \ln \theta' = \ln \theta - X \frac{\partial \ln \mu_0}{\partial X} \frac{\omega'_T}{\omega'_X}$$

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$$\text{with } \ln \theta' = \ln \theta - X \frac{\partial \ln \mu_0}{\partial X} \frac{\omega'_T}{\omega'_X}$$

$$\ln \theta' = \ln \theta - XL/c_p T_0 \quad \text{for moist convection}$$

- Generalisation of mixing length theory

Can define an **adiabatic convective flux**:

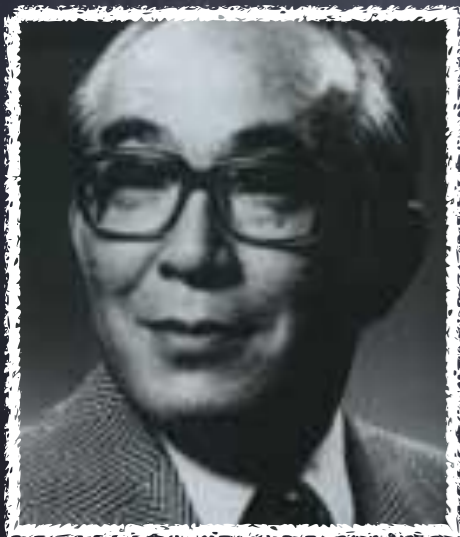
$$F_{\text{ad}} = \rho c_p w_{\text{ad}} T_0 (\nabla_T - \nabla_{\text{ad}})$$

or

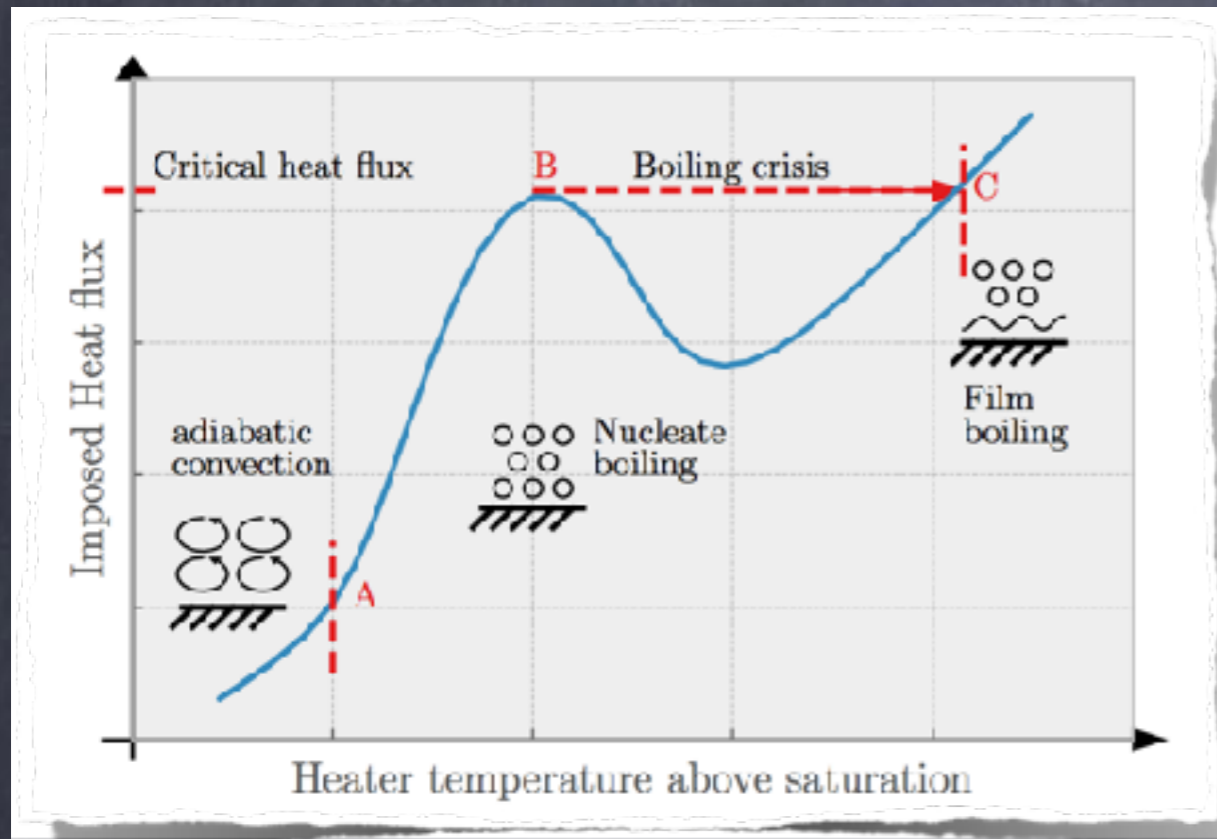
Can define a **diabatic convective flux**:

$$F_{\text{d}} = \rho c_p w_{\text{d}} T_0 (\nabla_T - \nabla_{\text{ad}} - \nabla_{\mu} \omega'_T / \omega'_X)$$

similar to mass/flux convection
parametrizations used for moist convection
(review: Arakawa & Jung 2011)

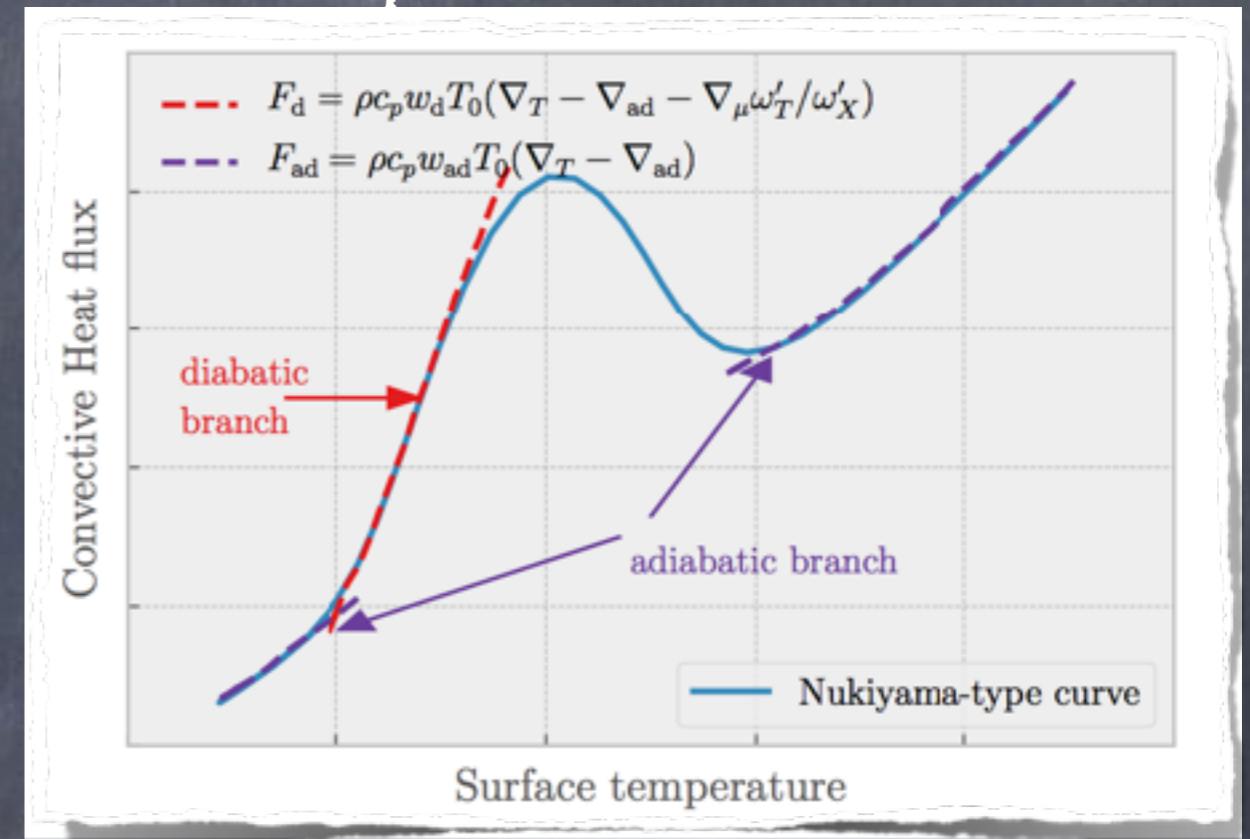
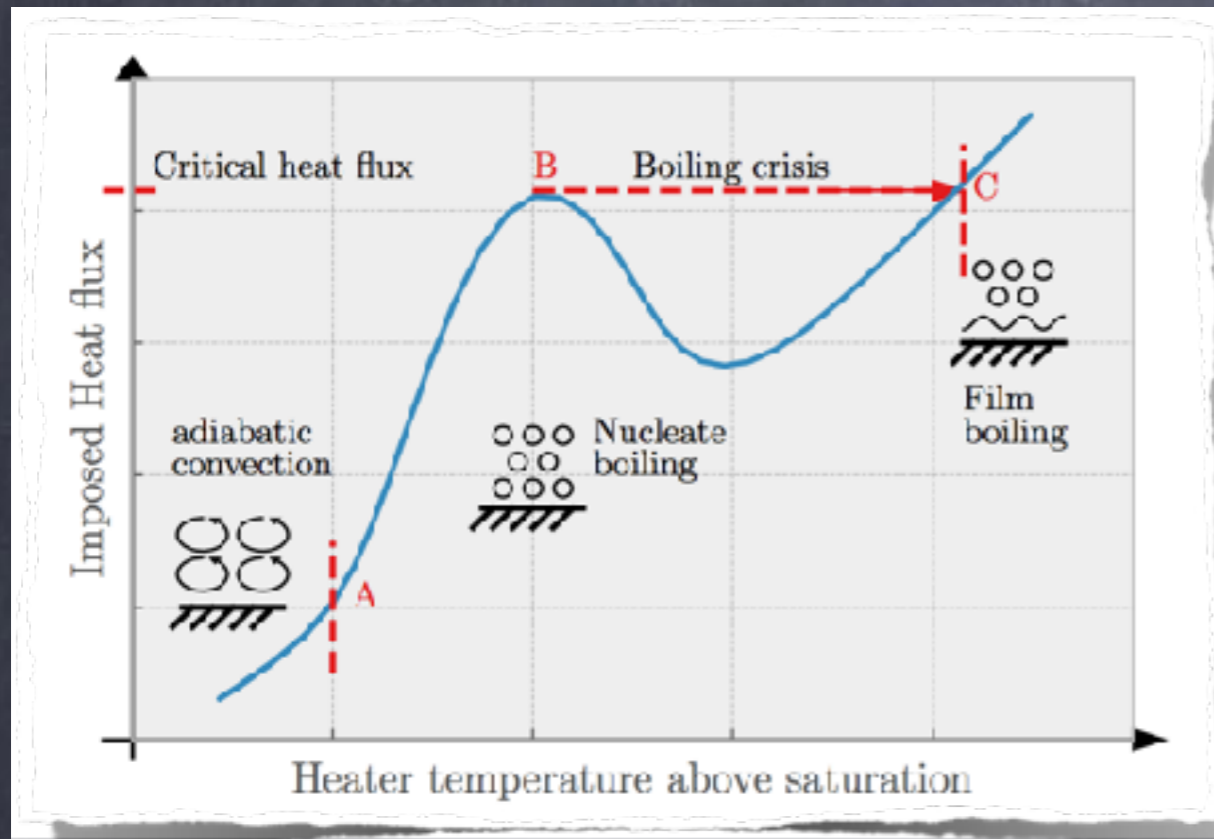


- **Bifurcation** between adiabatic and diabatic convection
- **Boiling crisis** in steam/liquid convection



Nukiyama 1934

- **Bifurcation** between adiabatic and diabatic convection
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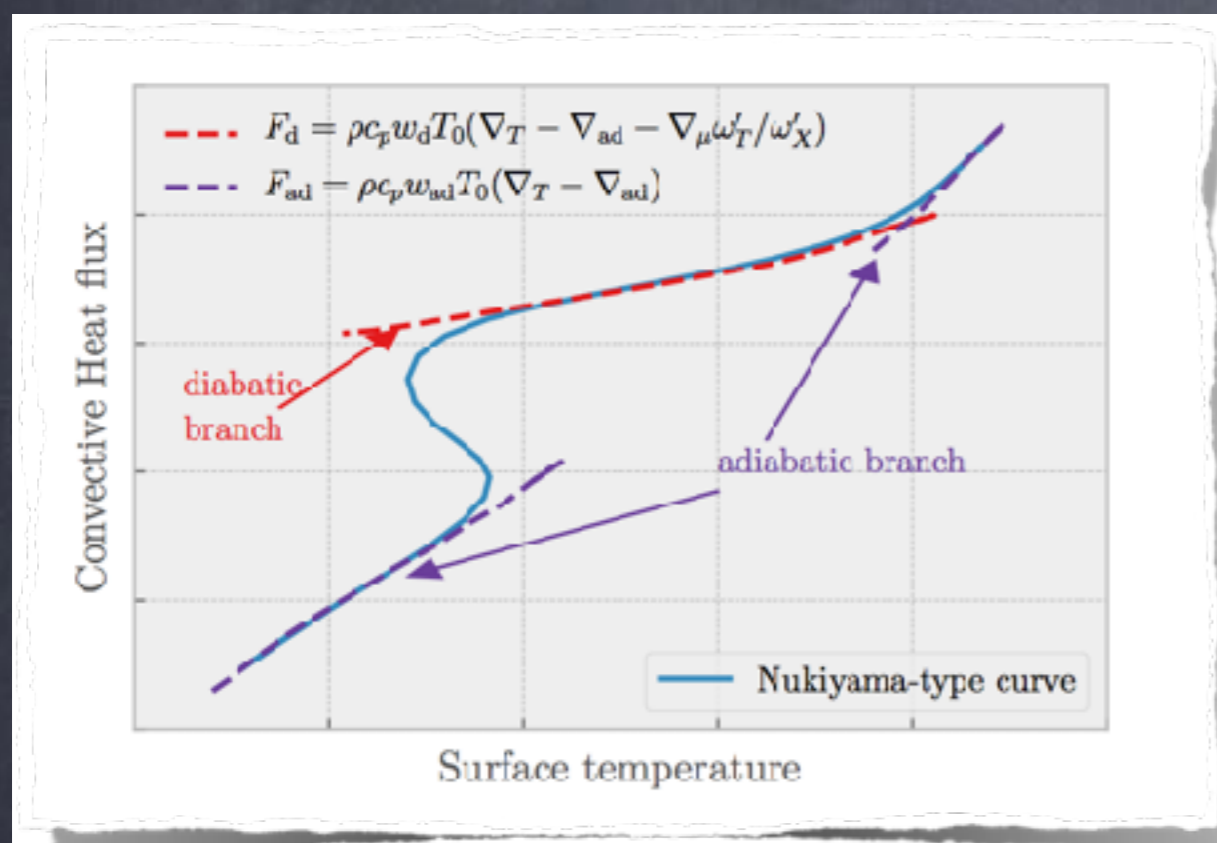


Nukiyama 1934

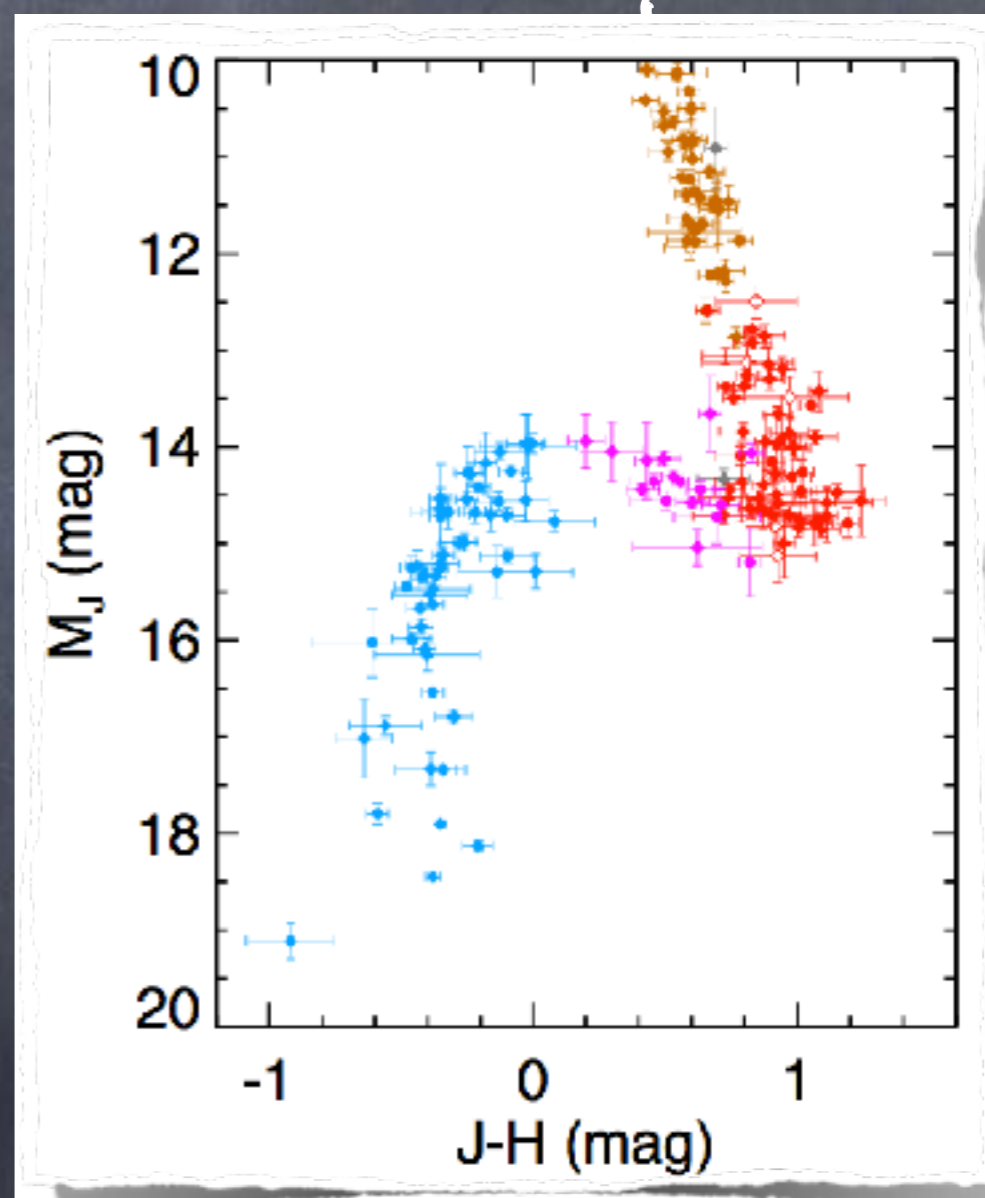
- Could provide a natural explanation of the boiling crisis?

- **Bifurcation** between adiabatic and diabatic convection

- **L/T transition** in brown-dwarf spectra?

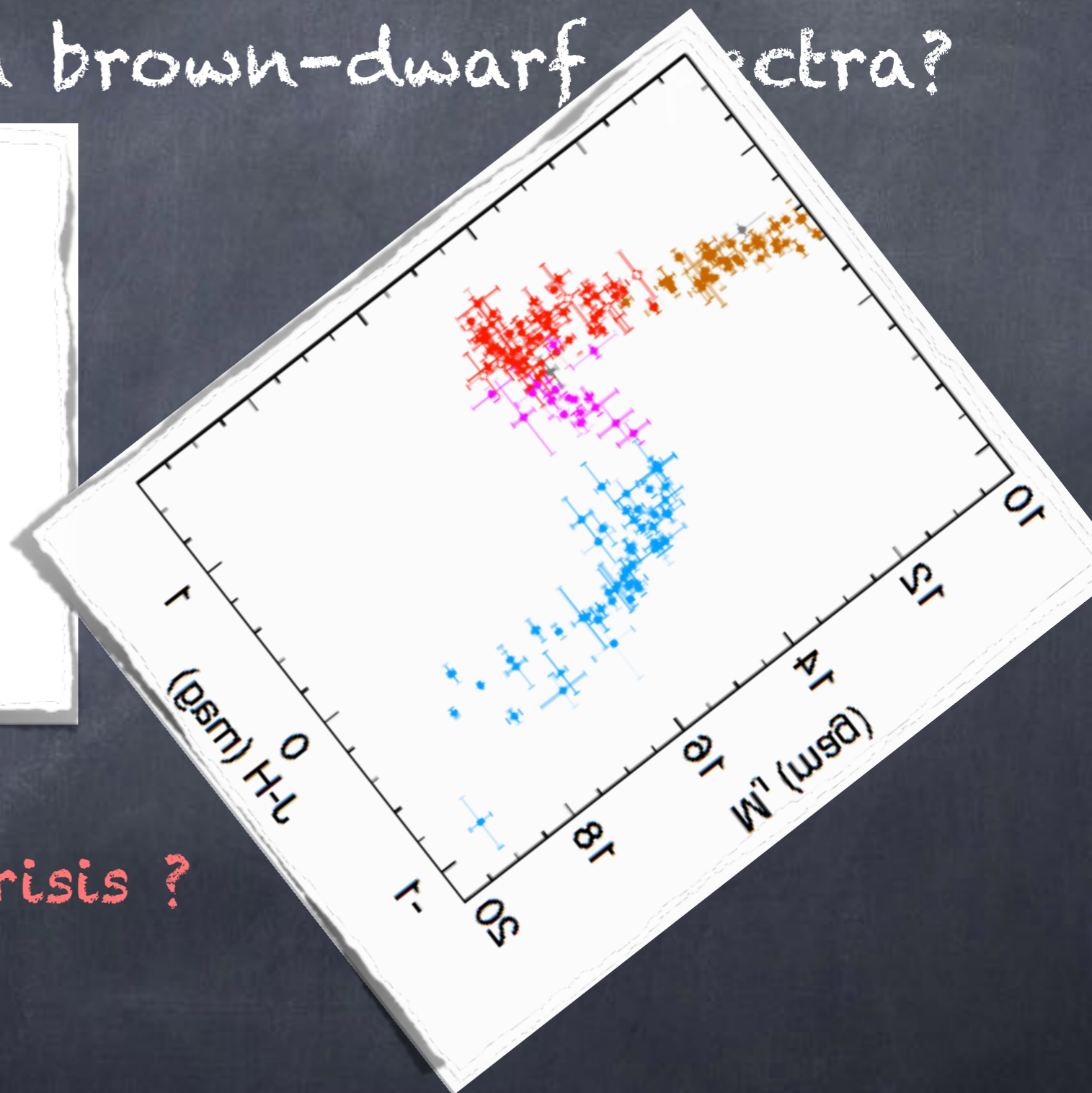
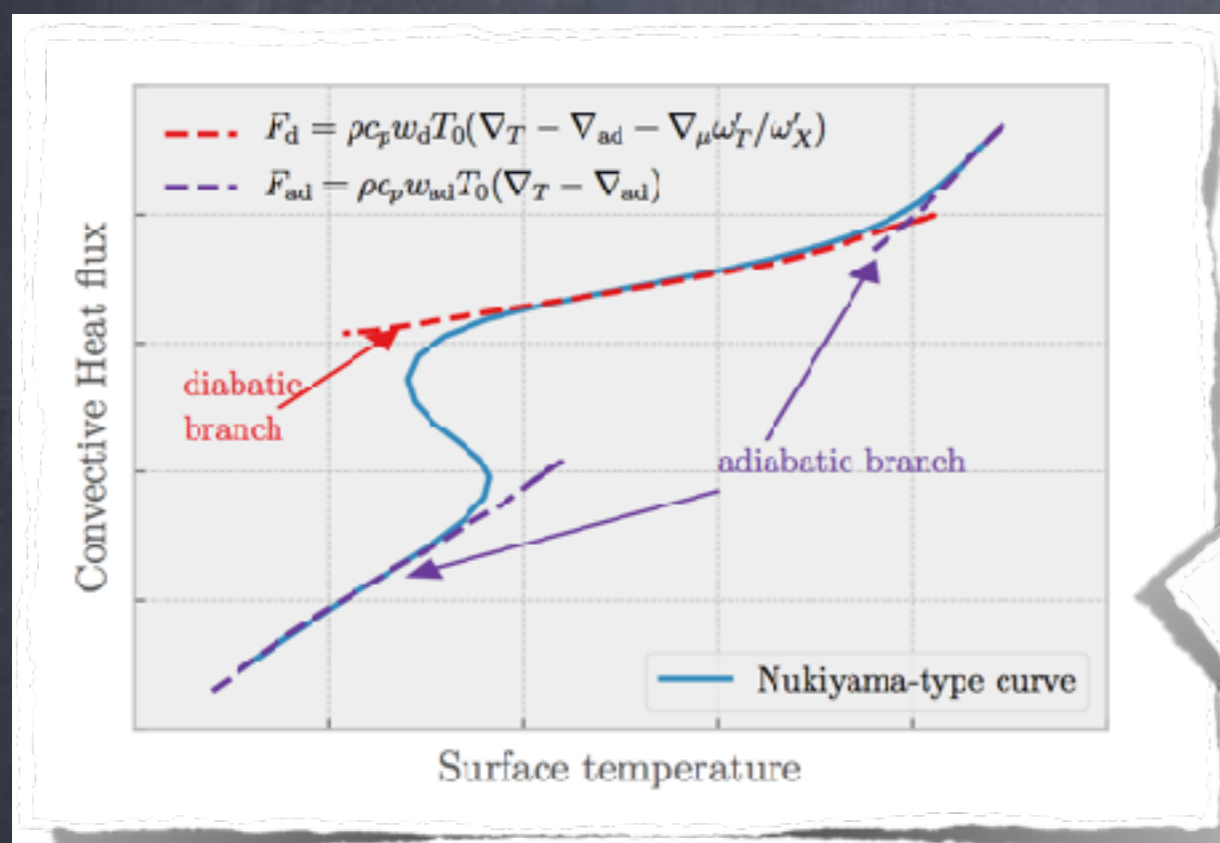


Dupuy & Liu 2012



- **Bifurcation** between adiabatic and diabatic convection

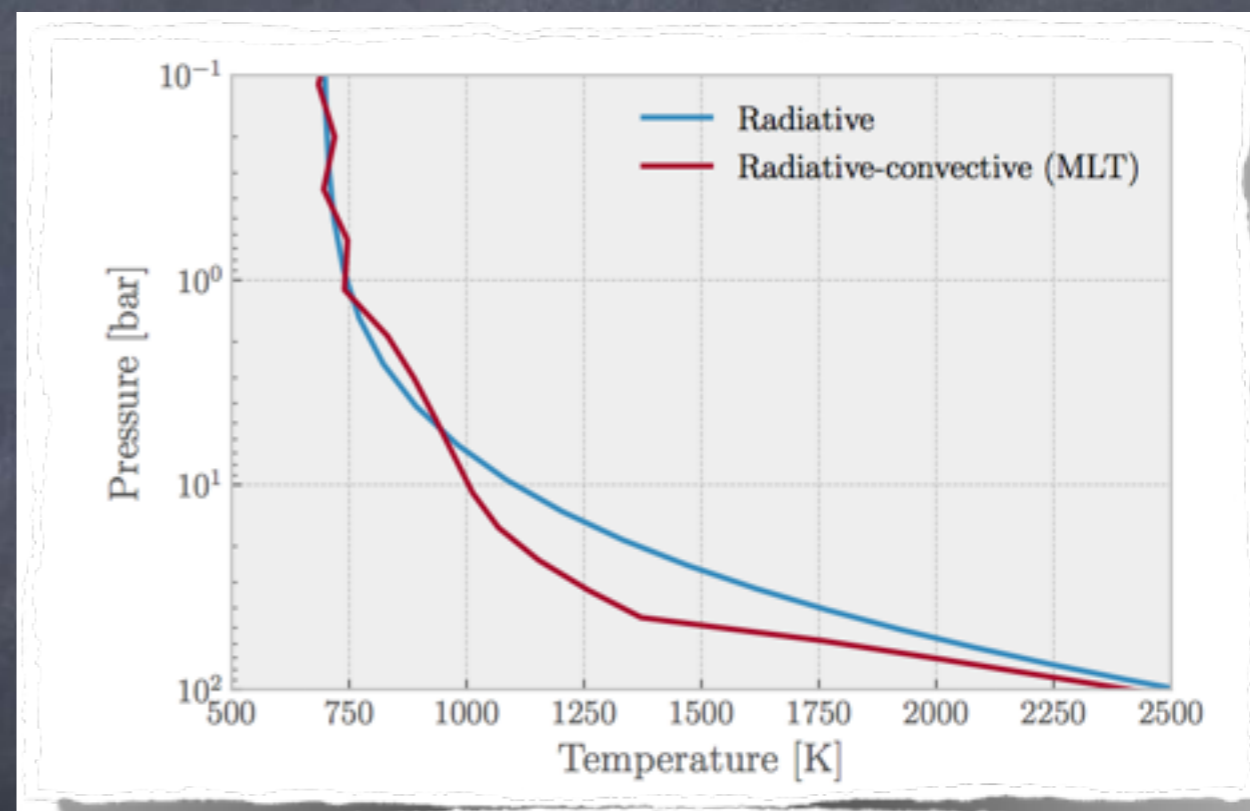
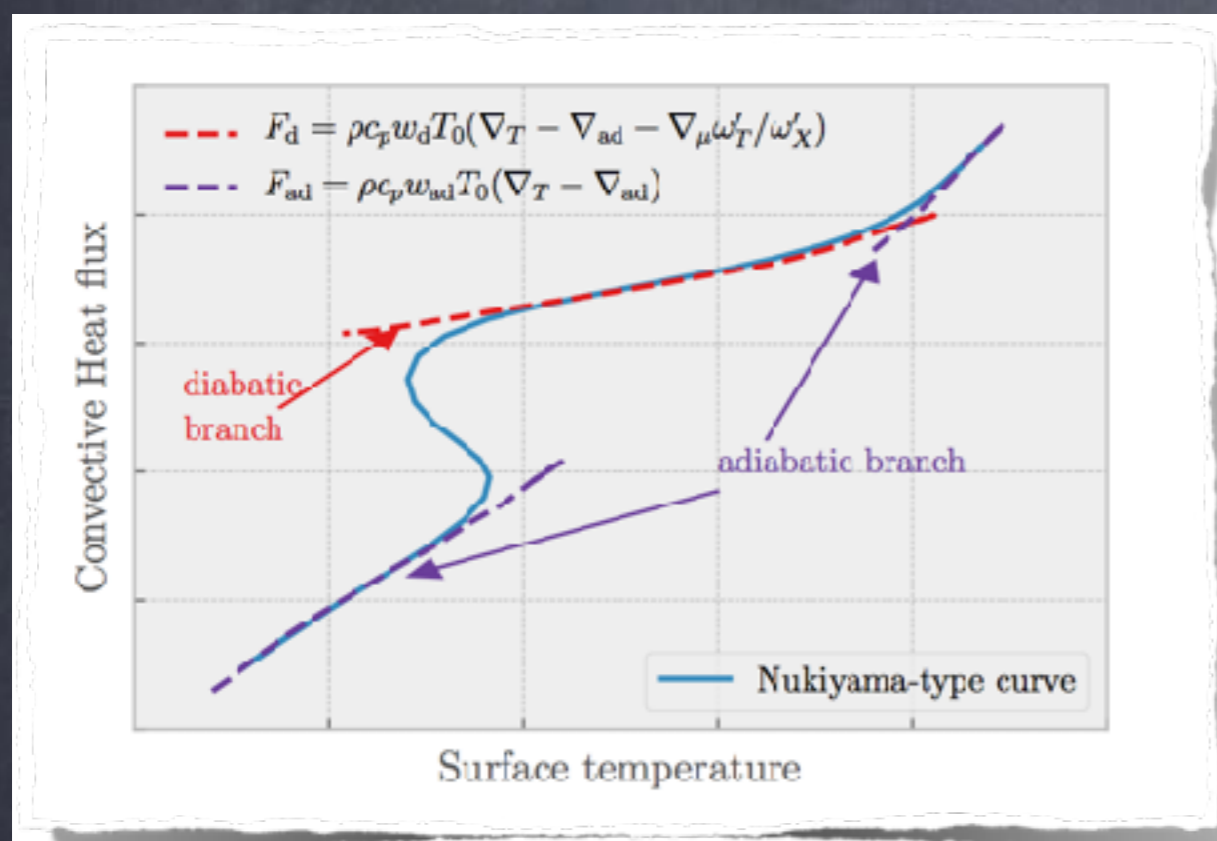
- **L/T transition** in brown-dwarf spectra?



A giant cooling crisis?

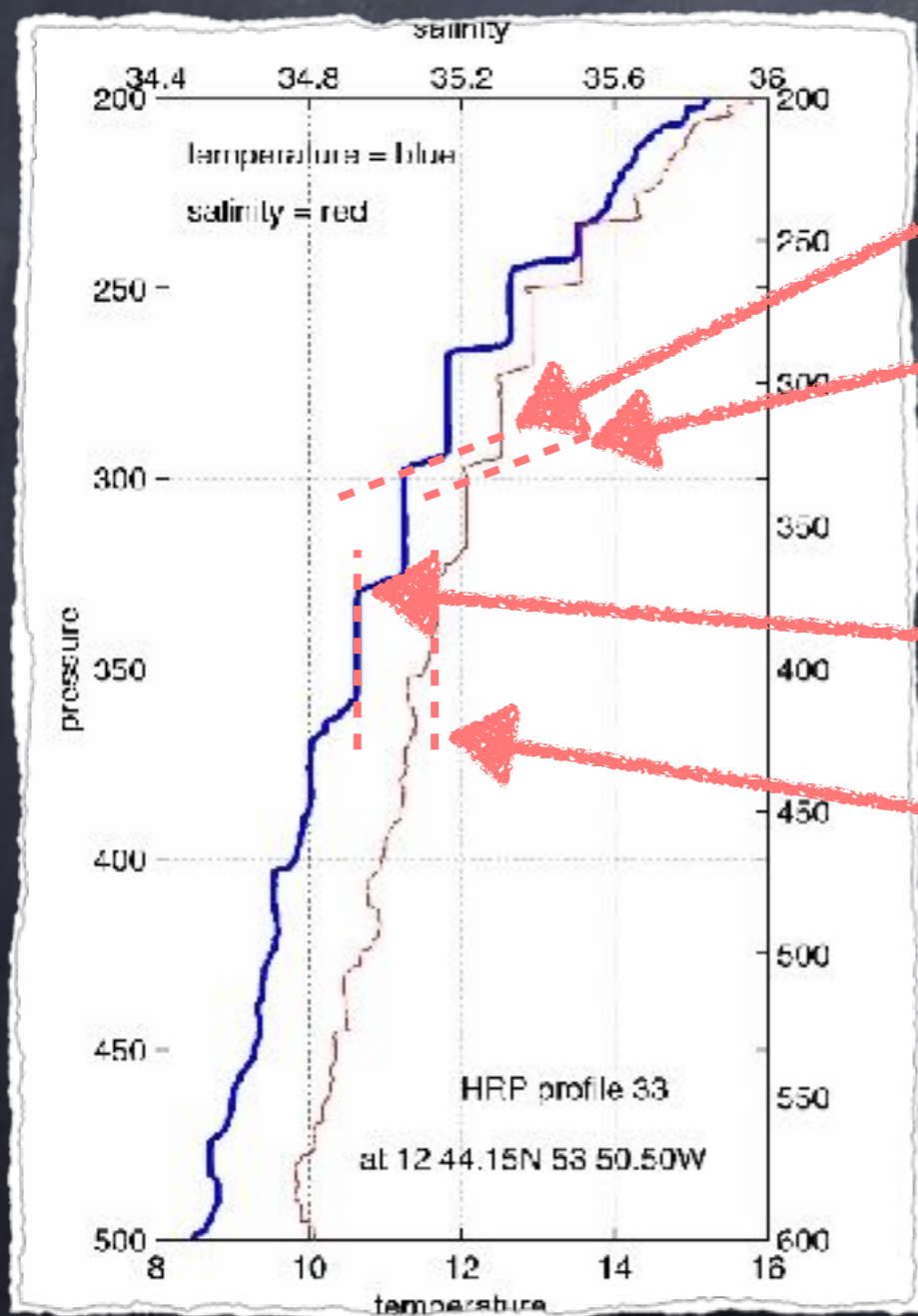
- **Bifurcation** between adiabatic and diabatic convection

- **L/T transition** in brown-dwarf spectra?



- **Bifurcation** between adiabatic and diabatic convection

- **Spatial** bifurcation: thermohaline staircase



$$F_d = \rho c_p w_d T_0 (\nabla_T - \nabla_{ad} - \nabla_\mu \kappa_T / \kappa_\mu)$$

$$X_d = \rho w_d \left(\frac{\partial \log \mu_0}{\partial X} \right)^{-1} (\nabla_\mu - (\nabla_T - \nabla_{ad}) \kappa_\mu / \kappa_T)$$

$$F_{ad} = \rho c_p w_{ad} T_0 (\nabla_T - \nabla_{ad})$$

$$X_{ad} = \rho w_{ad} \left(\frac{\partial \log \mu_0}{\partial X} \right)^{-1} (\nabla_\mu)$$

- Conclusions:

- Stratified **all-regime** compressible hydrodynamic solvers can be developed with efficient **HPC support (MPI+Kokkos)** to study these convective instabilities
- Thermohaline, fingering, moist, steam/liquid, CO/CH₄ radiative convection all derive from this diabatic branch of convection
- Extension at high order, implicit acoustic waves and radiative transfer (Trilinos)